

Features

- 1600 Wall System™2 is an outside glazed structurally silicone glazed curtain wall
- 1600 Wall System™2 has a 2-1/2" (63.5) sight line
- Standard 6" (152.4) or 7-1/2" (190.5) depth systems
- Standard infill options 1/4" (6.4) and 1" (25.4), other infills available
- Thermally Broken by means of a continuous 1/4" (6.4) low conductance spacer
- Concealed fastener joinery creates smooth, monolithic appearance
- Open-back horizontals and perimeters are available for cost savings
- Shear block fabrication method
- Corners and splayed mullions
- Offers integrated entrance framing systems
- Silicon compatible glazing materials for long-lasting seals
- 1600 Wall System™2 has been small and large missile impact and cycle tested
- Two color option
- Permanodic™ anodized finishes in seven choices
- Painted finishes in standard and custom choices

Optional Features

- Steel reinforcing
- Rain screen and backpans
- Optional deep profile and bull-nose covers
- Deep and heavy-weight mullions
- Fiberglass pressure plates
- Veneer system
- Integrates with standard Kawneer windows and GLASSvent™ windows for curtain wall
- Integrates with Versoleil™ SunShade Outrigger System and Horizontal Single Blade Systems
- Profit\$Maker™ Plus die sets
- Hurricane impact resistant framing option: 7-13/16" (198.4)

Product Applications

- Ideal for low to mid-rise applications where high performance is desired
- It is also the right choice for high span applications

For specific product applications,
consult your Kawneer representative.

Laws and building and safety codes governing the design and use of glazed entrance, window, and curtain wall products vary widely. Kawneer does not control the selection of product configurations, operating hardware, or glazing materials, and assumes no responsibility therefor.

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Architects – Most extrusion and window types illustrated in this catalog are standard products for Kawneer. These concepts have been expanded and modified to afford you design freedom. Some miscellaneous details are non-standard and are intended to demonstrate how the system can be modified to expand design flexibility. Please contact your Kawneer representative for further assistance.

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LAWS AND BUILDING AND SAFETY CODES GOVERNING THE DESIGN AND USE OF GLAZED ENTRANCE, WINDOW, AND CURTAIN WALL PRODUCTS VARY WIDELY. KAWNEER DOES NOT CONTROL THE SELECTION OF PRODUCT CONFIGURATIONS, OPERATING HARDWARE, OR GLAZING MATERIALS, AND ASSUMES NO RESPONSIBILITY THEREFOR.

Metric (SI) conversion figures are included throughout these details for reference. Numbers in parentheses () are millimeters unless otherwise noted.

The following metric (SI) units are found in these details:

m – meter
 cm – centimeter
 mm – millimeter
 s – second
 Pa – pascal
 MPa – megapascal

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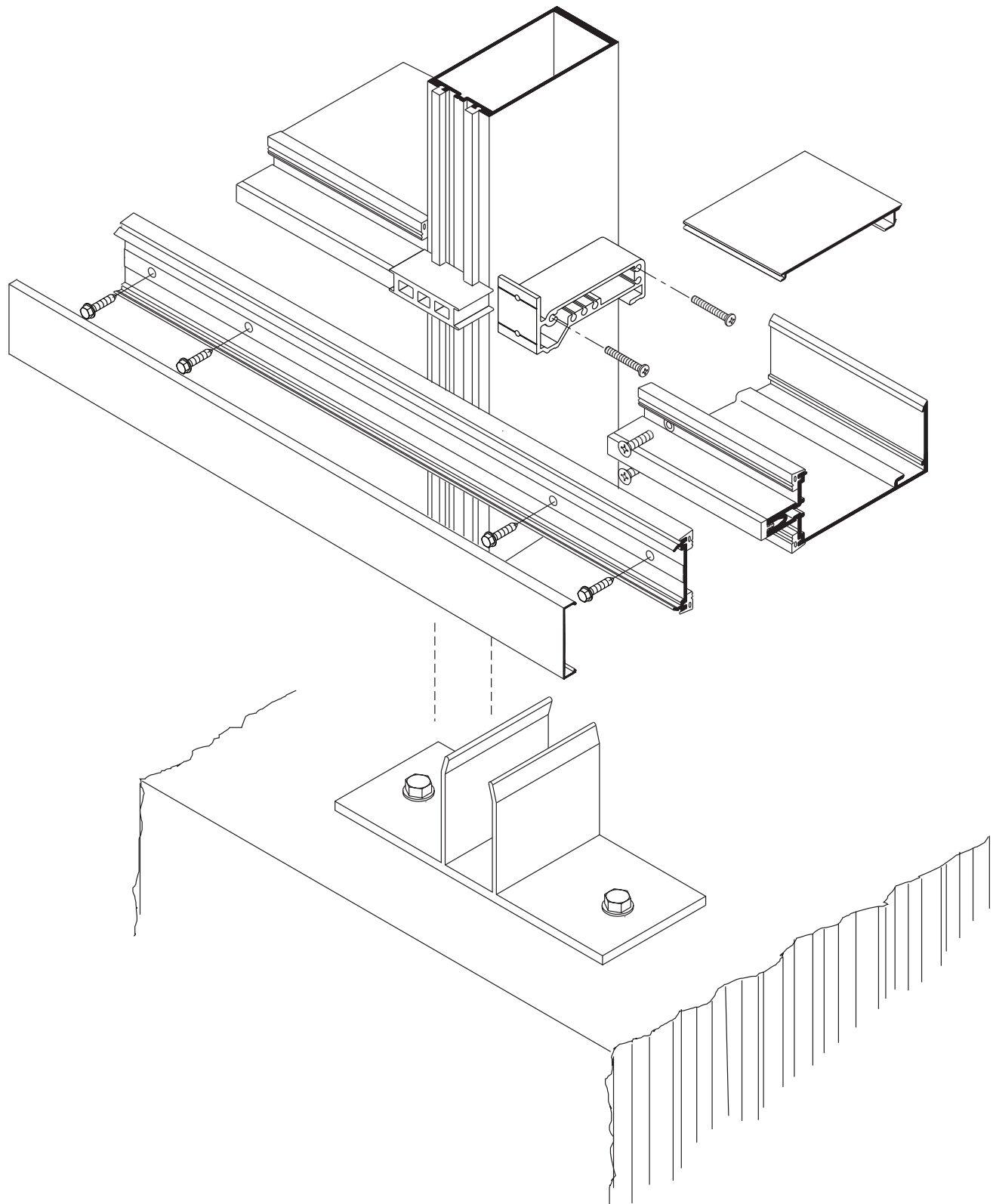
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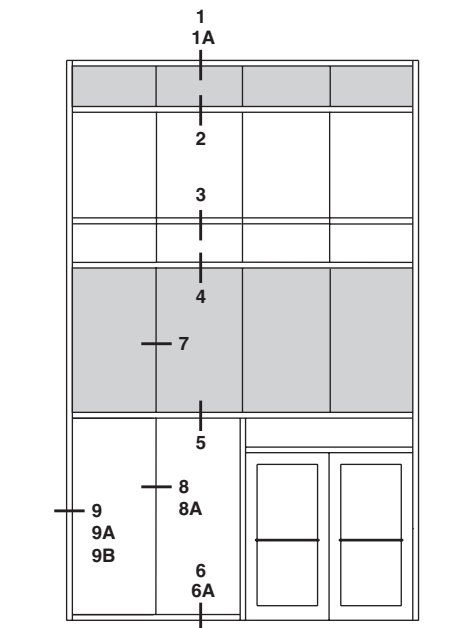


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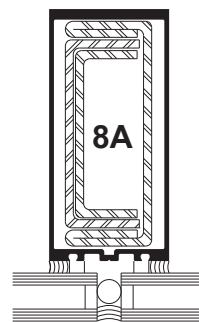
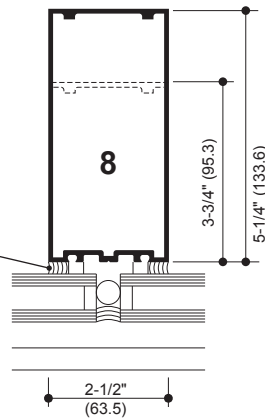
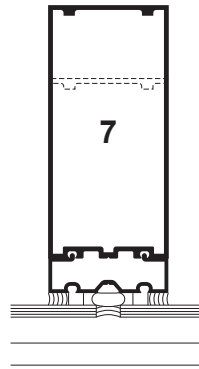
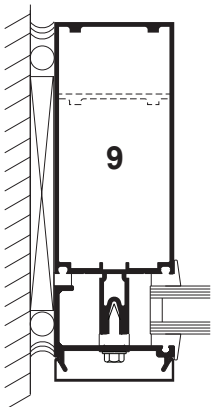
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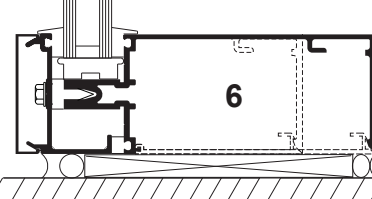
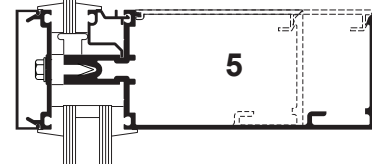
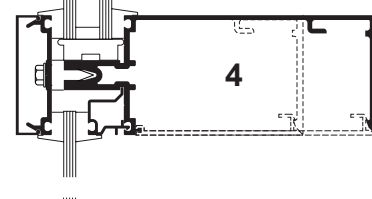
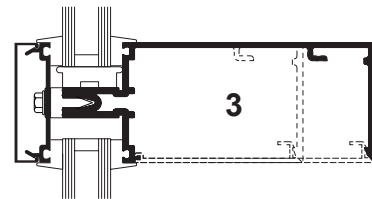
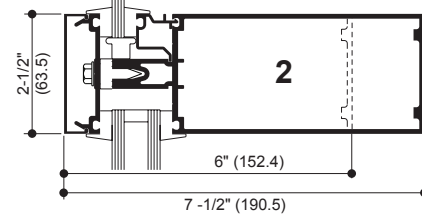
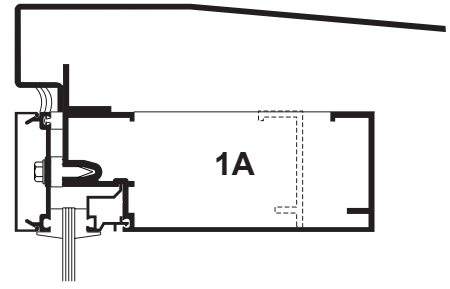
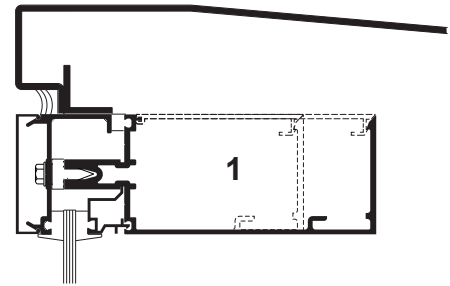
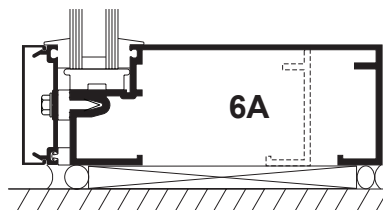
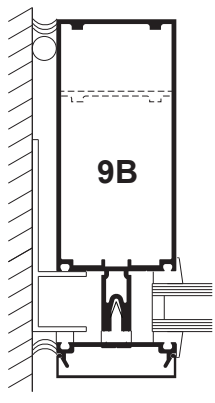
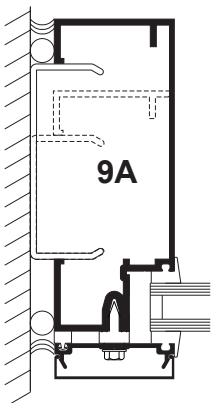


ELEVATION IS NUMBER KEYED TO DETAILS

Structural Silicone Sealant
(by Others)*



OPTIONAL STEEL
REINFORCING
AS REQUIRED



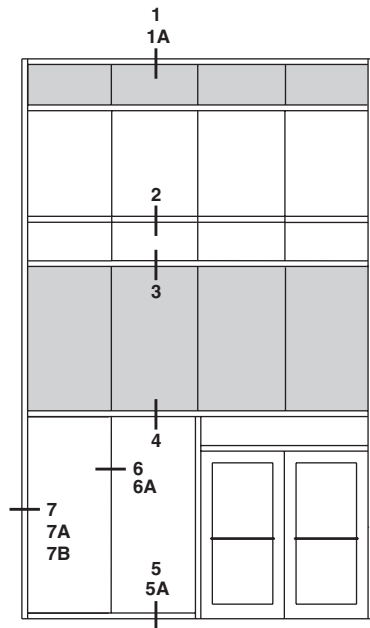
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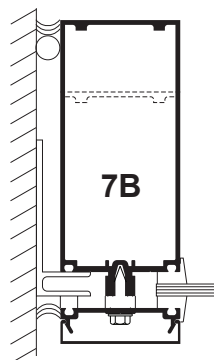
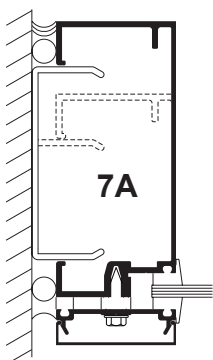
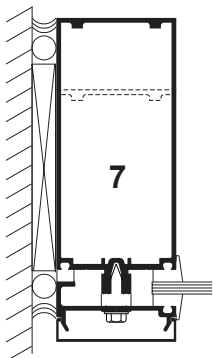
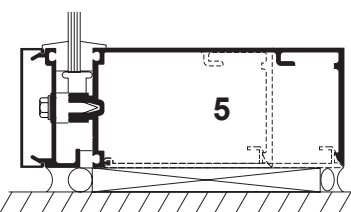
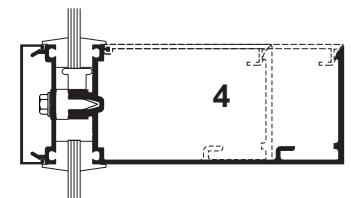
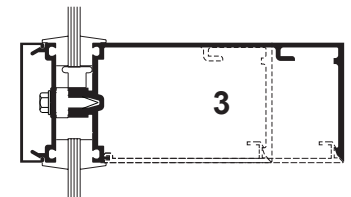
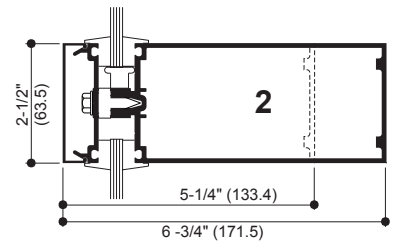
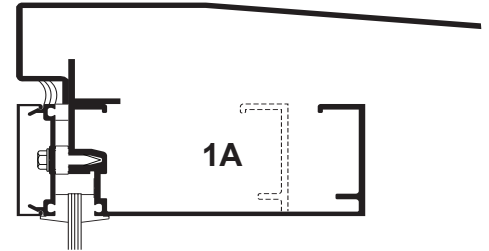
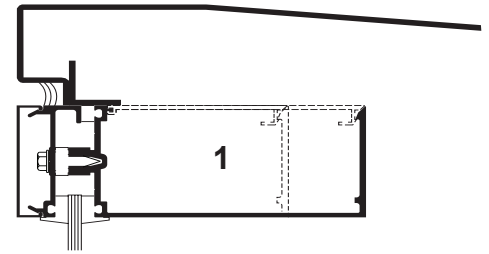
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* INSTALLER NOTE: Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

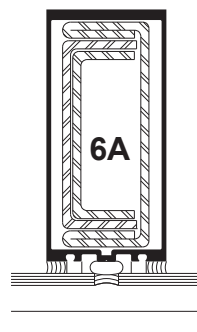
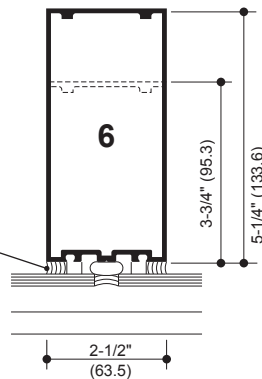
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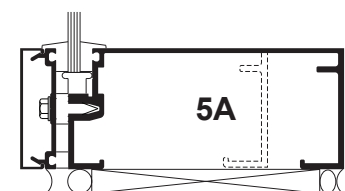
ELEVATION IS NUMBER KEYED TO DETAILS



Structural Silicone Sealant
(by Others)*



OPTIONAL STEEL
REINFORCING
AS REQUIRED



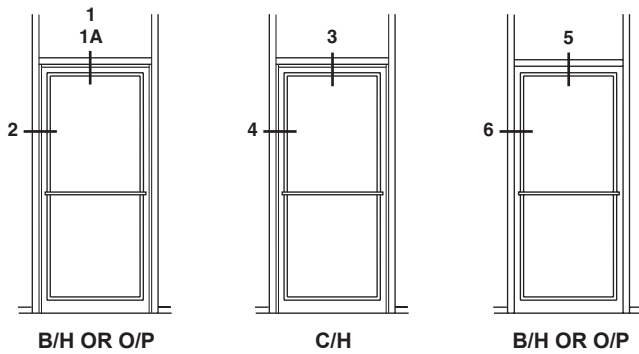
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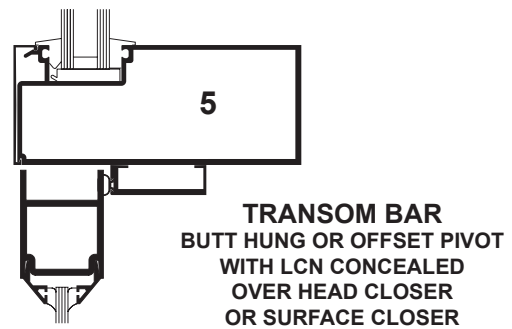
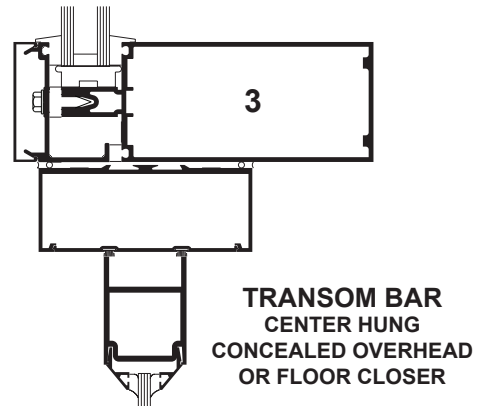
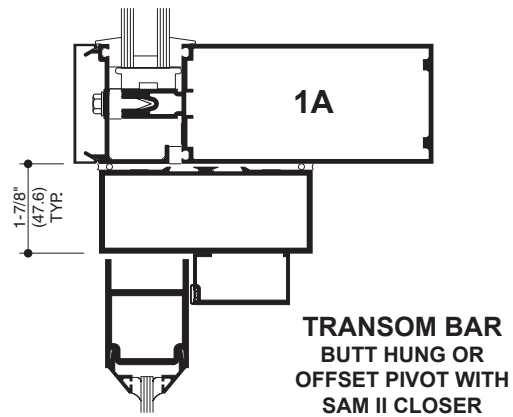
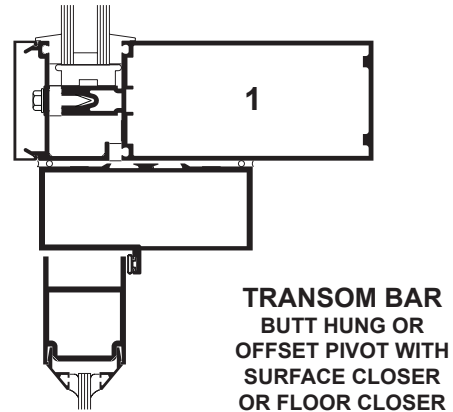
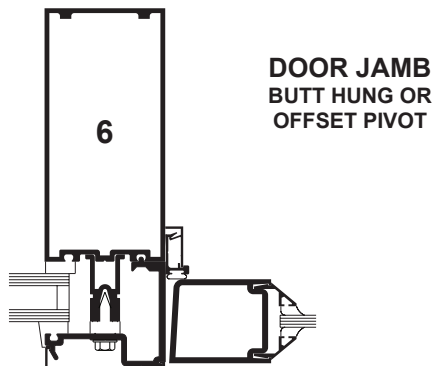
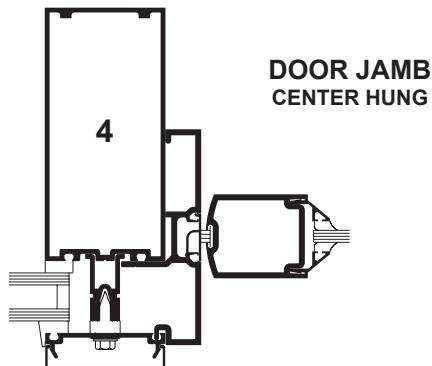
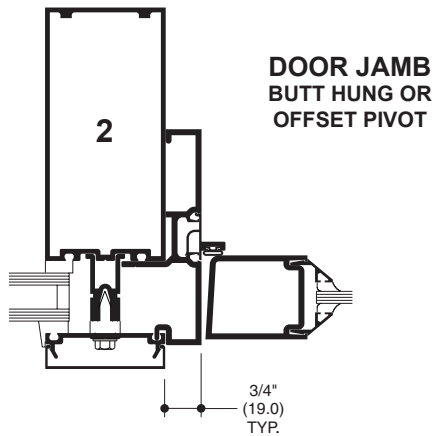
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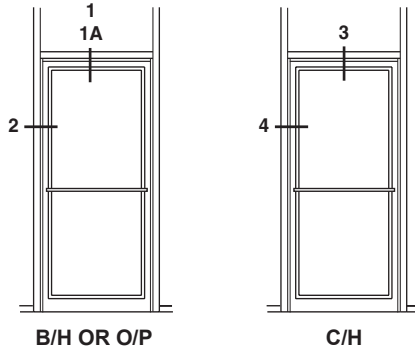


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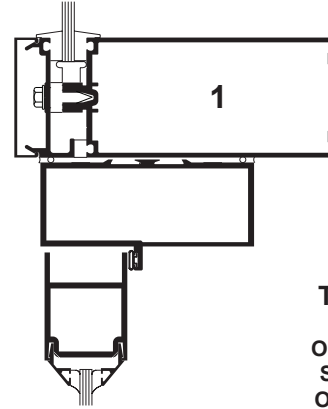
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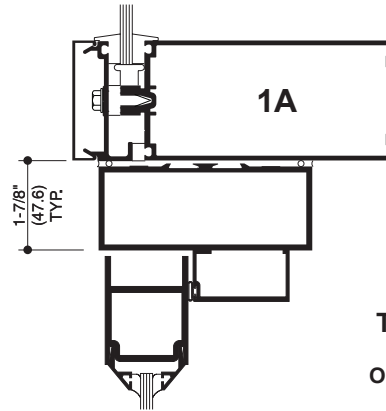
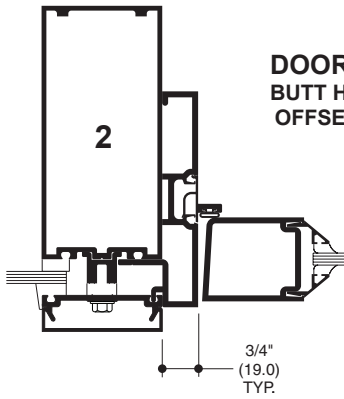
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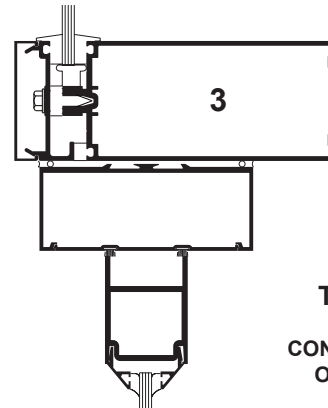
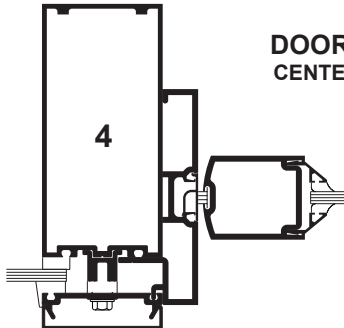
ELEVATION IS NUMBER KEYED TO DETAILS



TRANSOM BAR
BUTT HUNG OR
OFFSET PIVOT WITH
SURFACE CLOSER
OR FLOOR CLOSER



TRANSOM BAR
BUTT HUNG OR
OFFSET PIVOT WITH
SAM II CLOSER



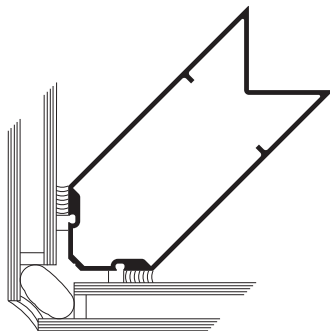
TRANSOM BAR
CENTER HUNG
CONCEALED OVERHEAD
OR FLOOR CLOSER

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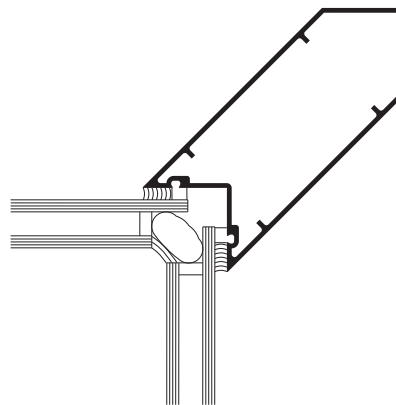
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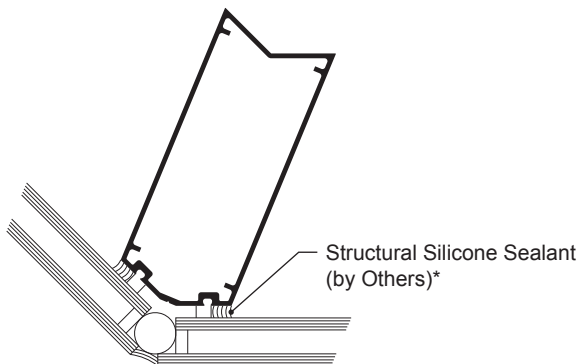
NOTE: 1" SYSTEM SHOWN, 1/4" SYSTEM SIMILAR.



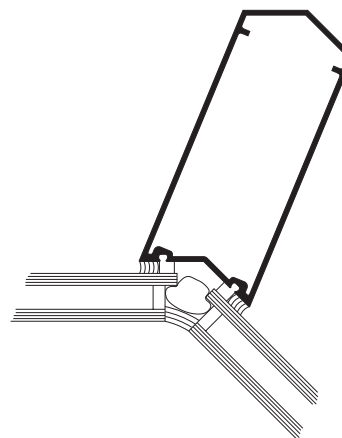
90° OUTSIDE CORNER



90° INSIDE CORNER



135° OUTSIDE CORNER



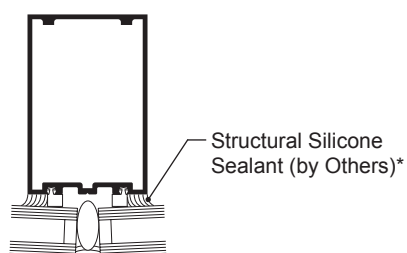
135° INSIDE CORNER

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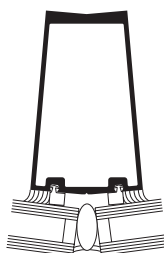
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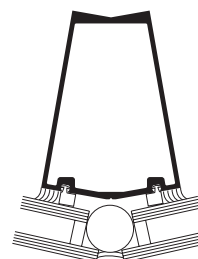
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0° TO 5°

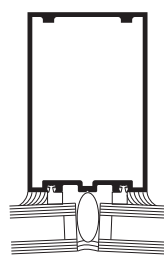


5° TO 15°

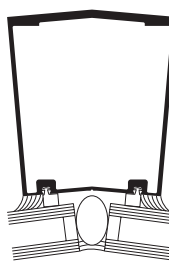


15° TO 25°

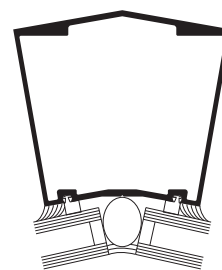
OUTSIDE SPLAYED MULLIONS



0° TO 5°



5° TO 15°

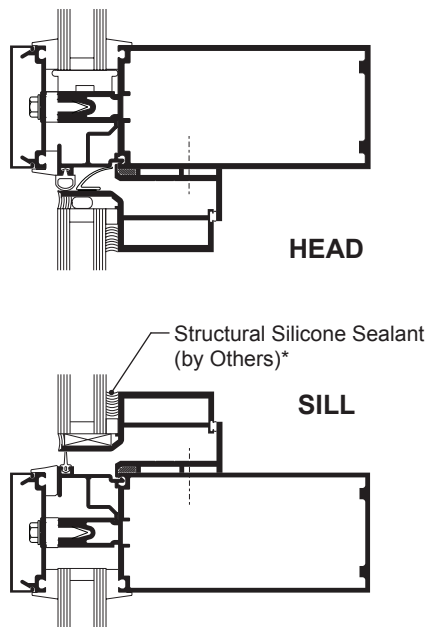


15° TO 25°

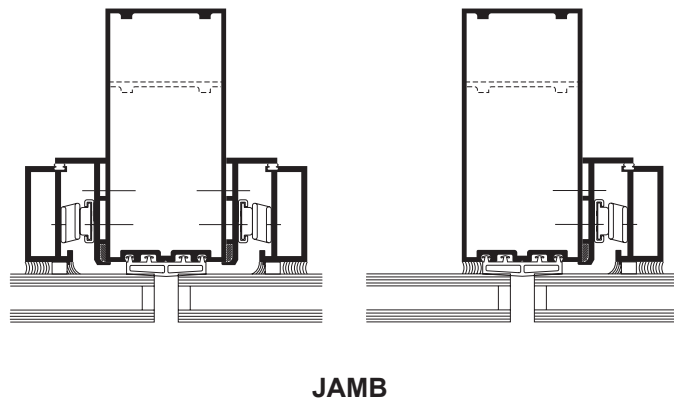
INSIDE SPLAYED MULLIONS

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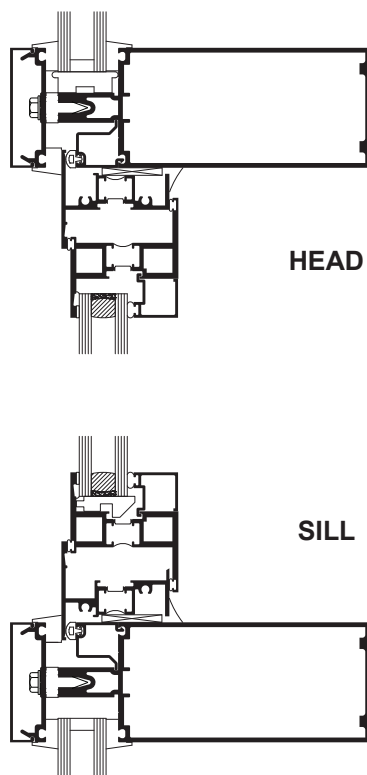
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GLASSvent™ WINDOWS FOR CURTAIN WALL

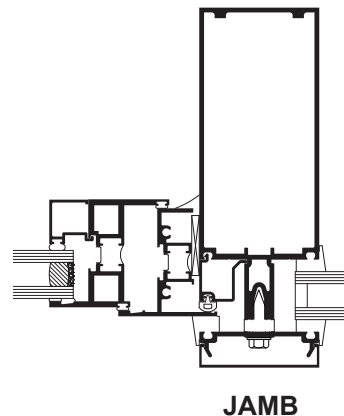


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8225TL THERMAL WINDOWS

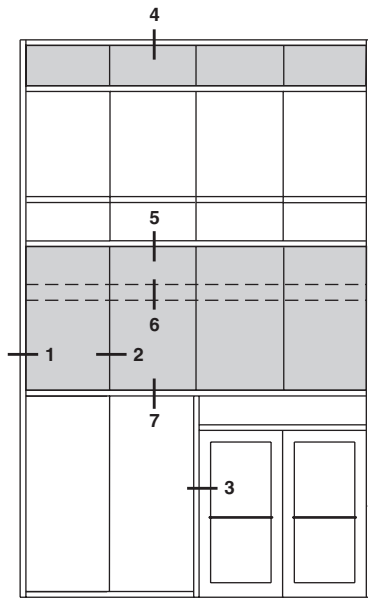
NOTE: Other vent types can be accommodated.
Contact your Kawneer representative for other options.



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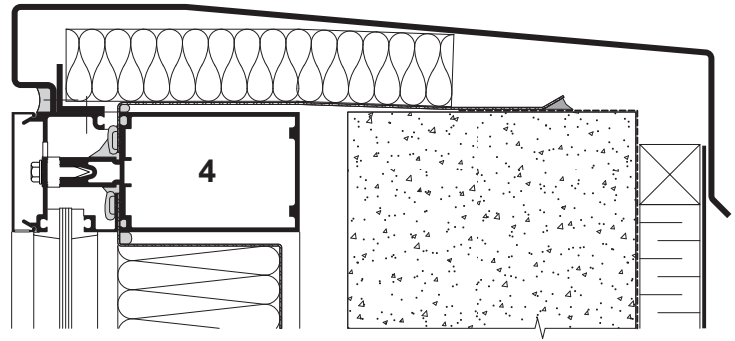
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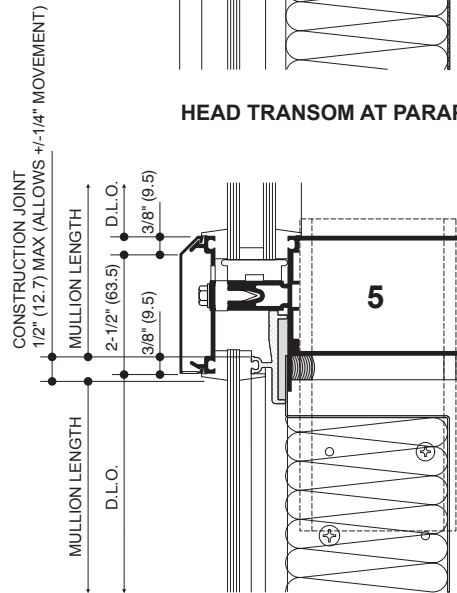


ELEVATION IS NUMBER KEYED TO DETAILS

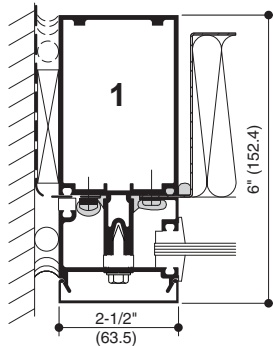
NOTE: 6" SYSTEM SHOWN, 7-1/2" SYSTEM SIMILAR



HEAD TRANSOM AT PARAPET FLASHING

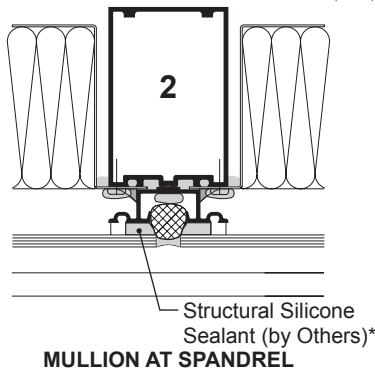


EXPANSION JOINT

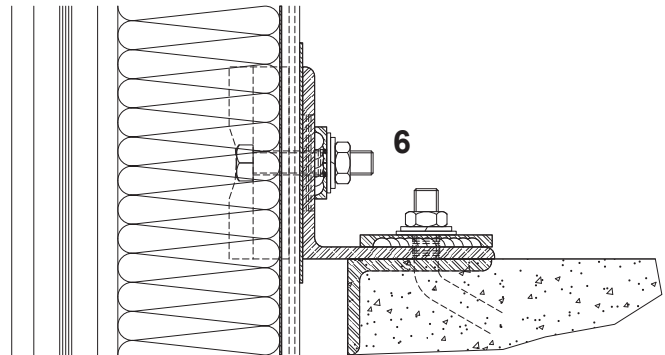


JAMB MULLION
AT SPANDREL

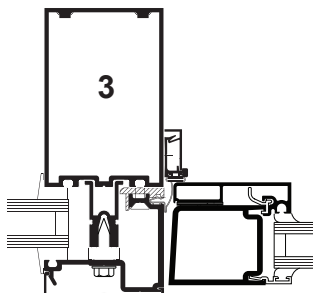
(With vapor barrier tie-in)



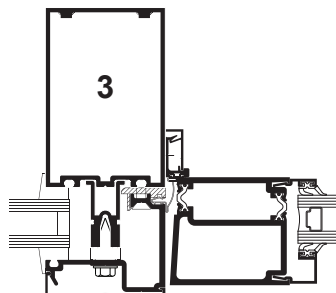
MULLION AT SPANDREL



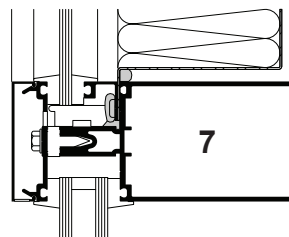
TYPICAL DEADLOAD ANCHOR



THERMALLY BROKEN
DOOR ADAPTOR
FOR INSULCLAD DOORS



AA™ 250 THERMAL
ENTRANCE

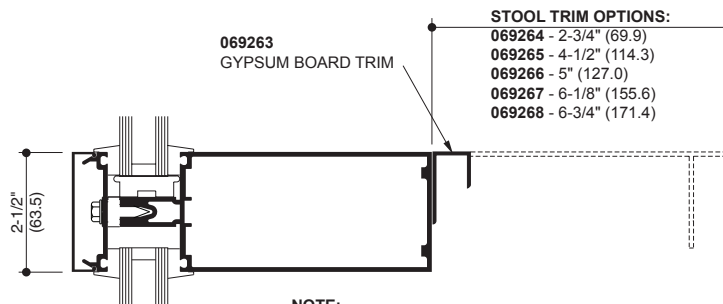
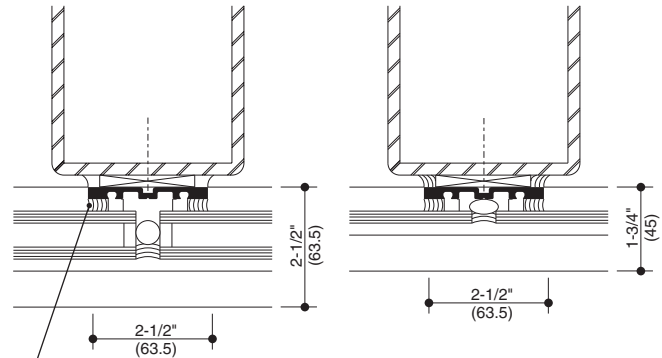
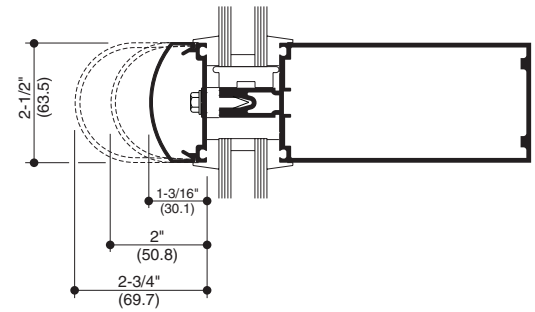
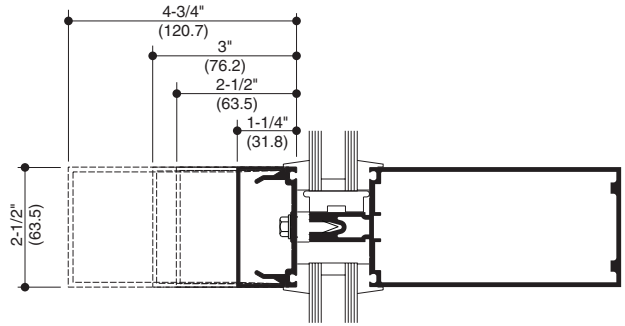
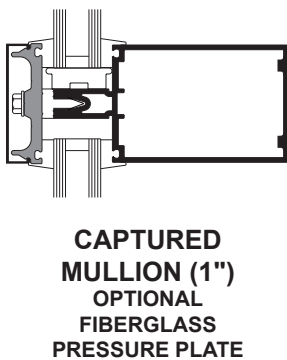
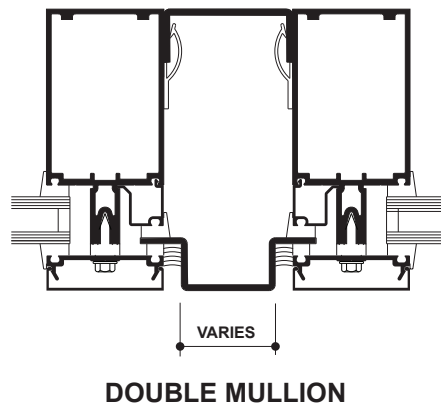
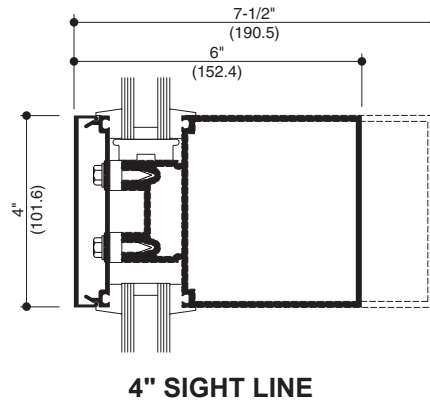
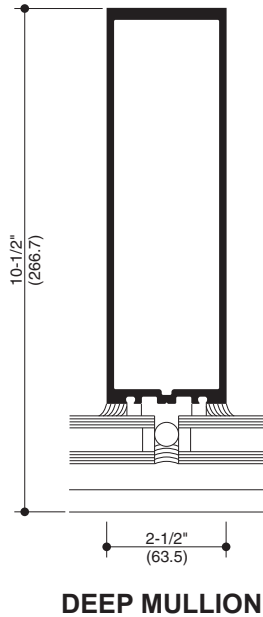


TRANSOM - SPANDREL OVER VISION

* **INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

Additional information and CAD details are available at www.kawneer.com

Architects – Most extrusion and window types illustrated in this catalog are standard products for Kawneer. These concepts have been expanded and modified to afford you design freedom. Some miscellaneous details are non-standard and are intended to demonstrate how the system can be modified to expand design flexibility. Please contact your Kawneer representative for further assistance.



INTERIOR STOOL TRIM

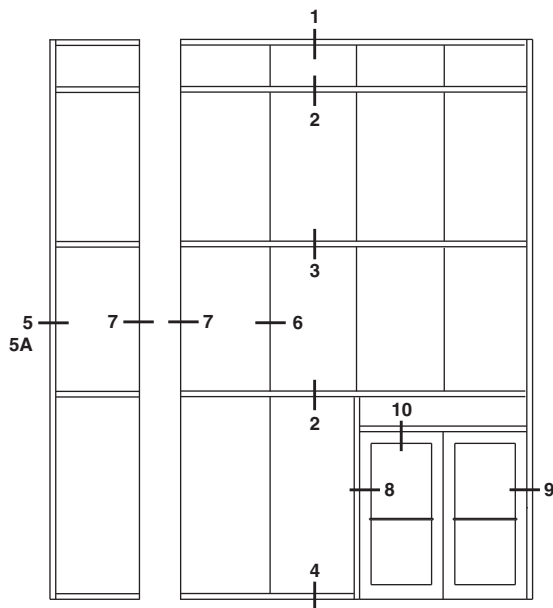
* **INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

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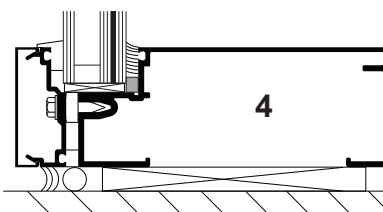
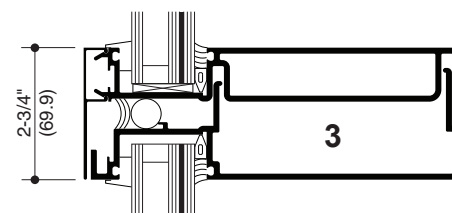
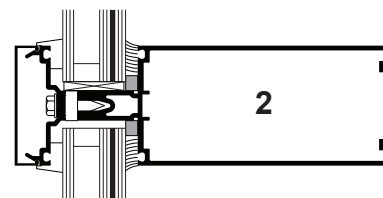
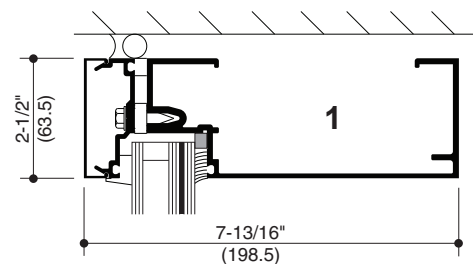
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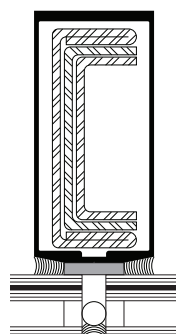
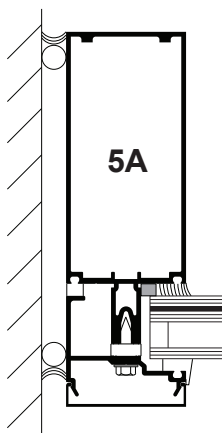
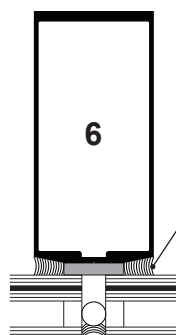
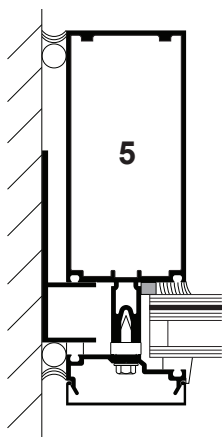
NOTE: DETAILS SHOWN WITH 1-5/16" INFILL AND ARE GLAZED FOR LARGE MISSILE IMPACT (LMI).
SEE NEXT PAGE FOR OTHER GLAZING OPTIONS.



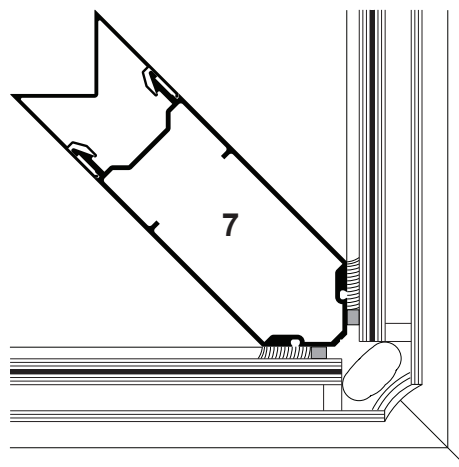
ELEVATION IS NUMBER KEYED TO DETAILS



EXPANSION
HORIZONTAL



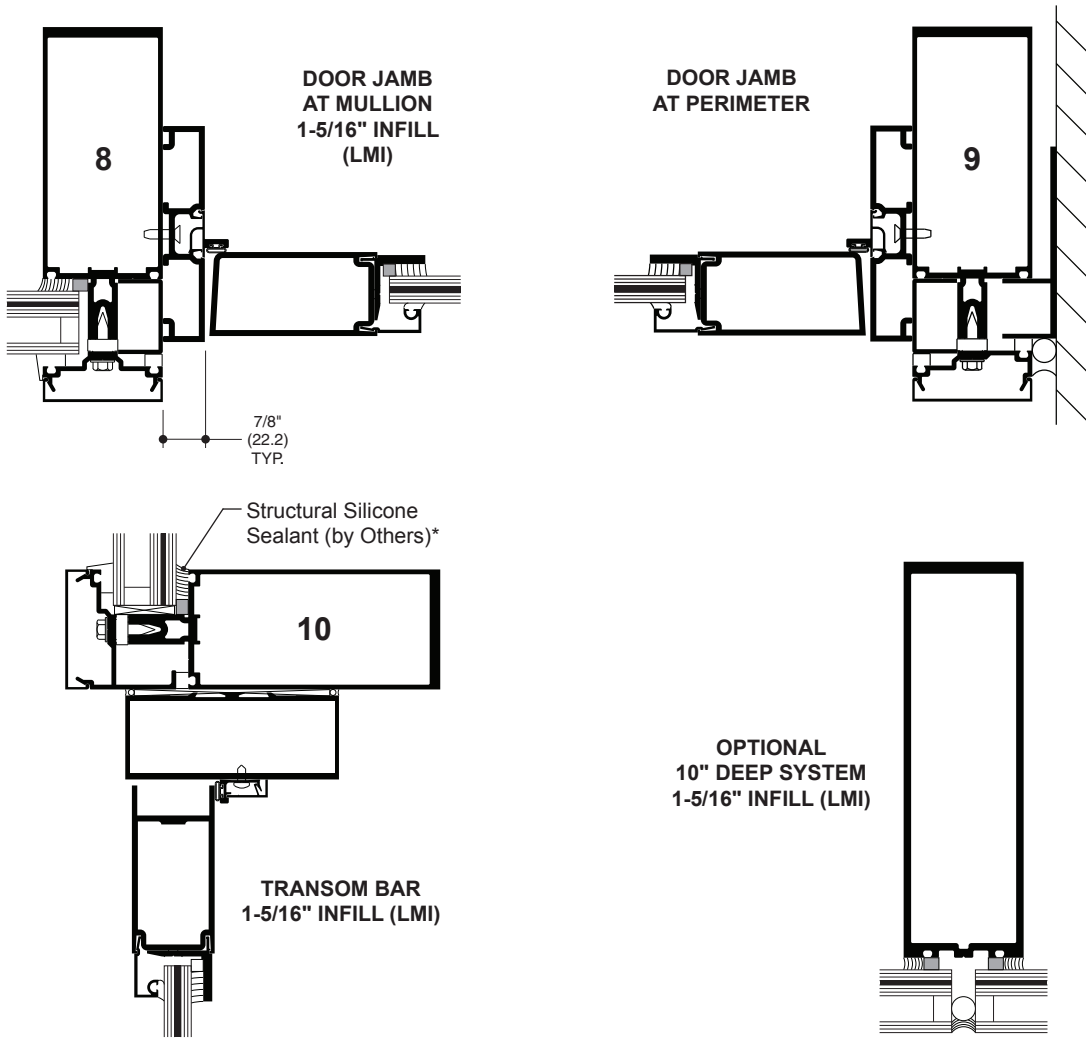
OPTIONAL STEEL
REINFORCING
AS REQUIRED



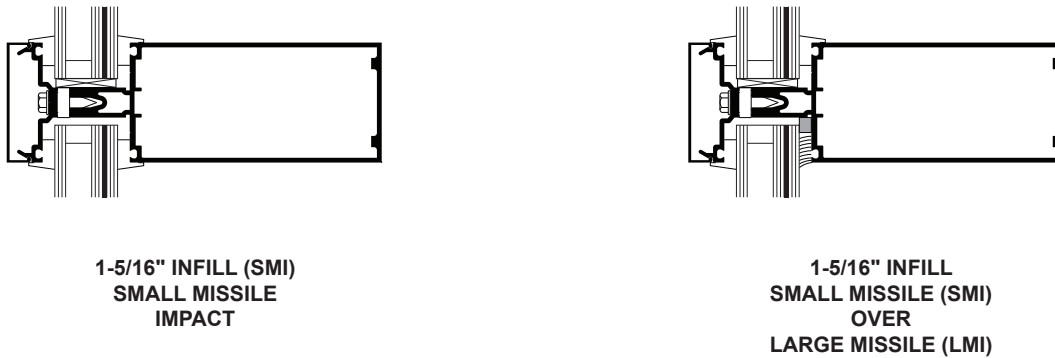
* **INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

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NOTE: 350 IR DOORS ARE USED WITH IMPACT FRAMING.
DOORS ARE GLAZED WITH 9/16" INFILL.

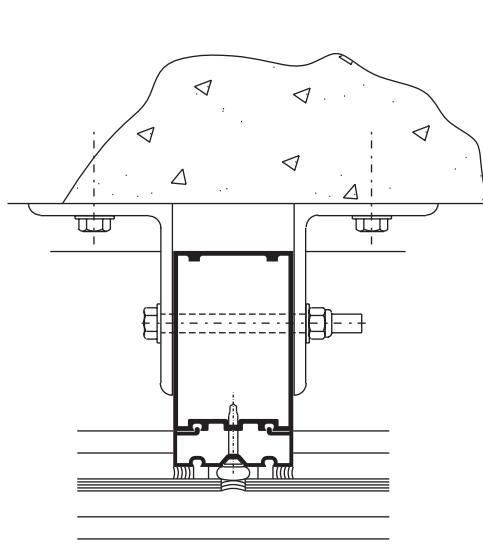


GLAZING OPTIONS

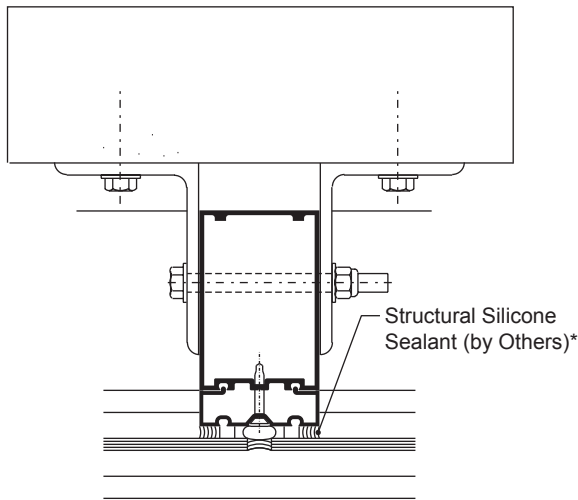
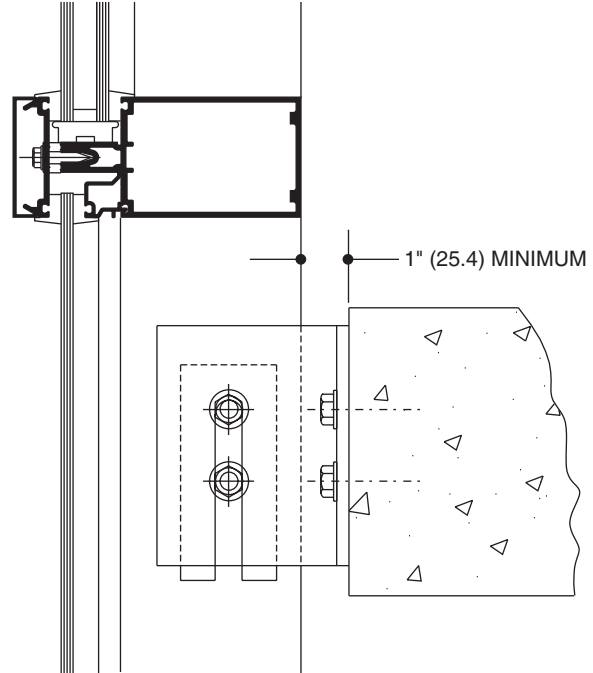


* **INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

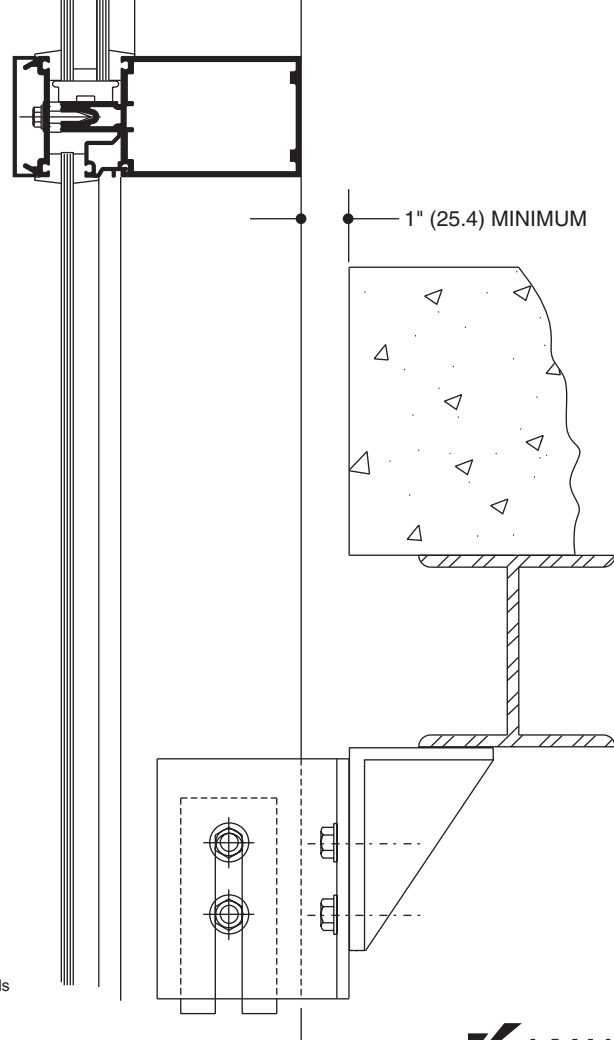
Actual project conditions will determine specific anchor design. Details on this page are for reference only.



ANCHORING TO FLOOR SLAB

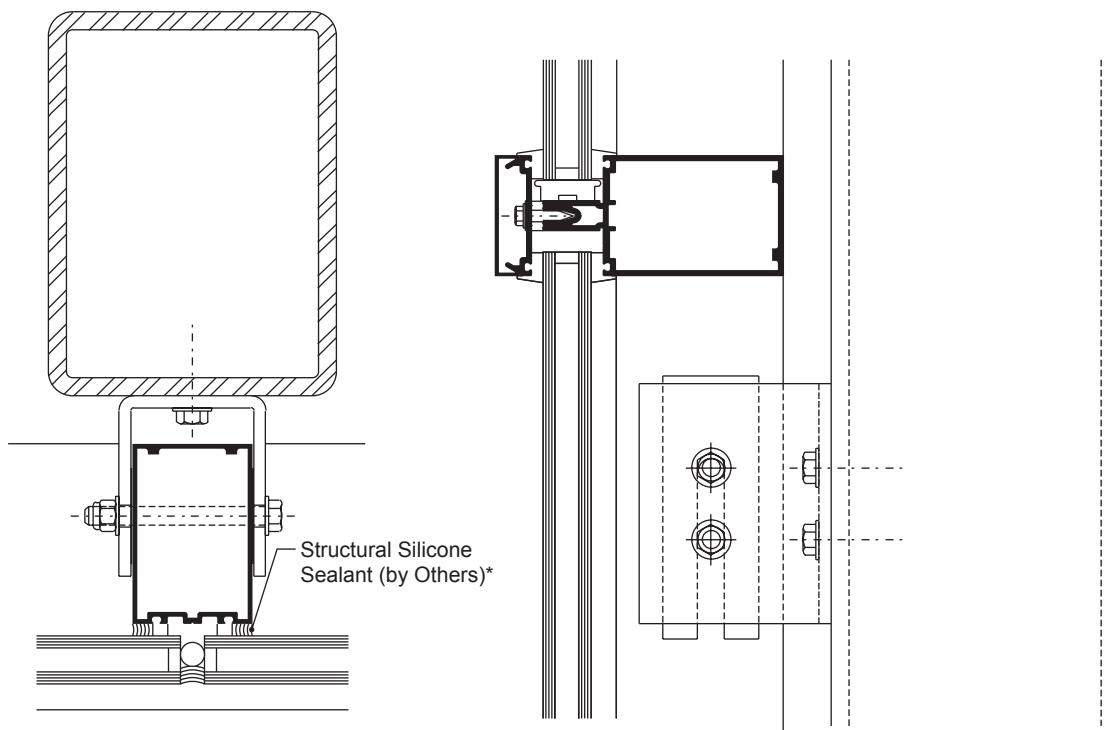
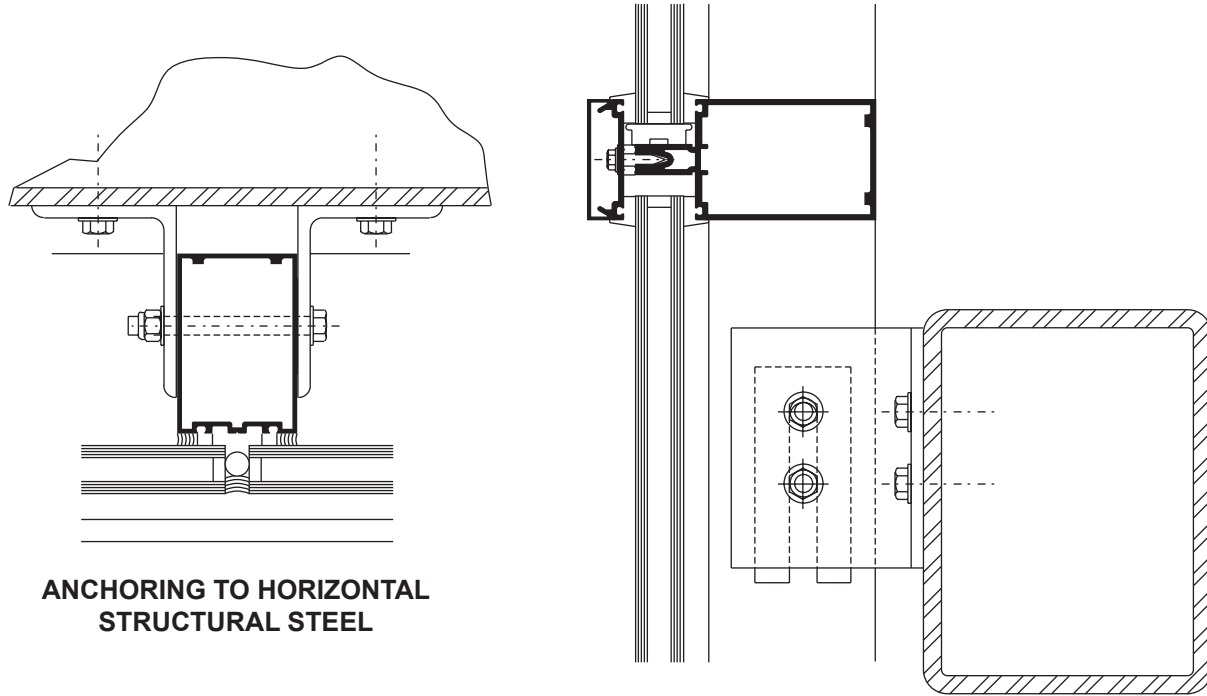


ANCHORING TO SUPPORT STEEL



*** INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

Actual project conditions will determine specific anchor design. Details on this page are for reference only.



* **INSTALLER NOTE:** Installer is responsible for all required compatibility review and approvals with the Structural Silicone Manufacturer and the Insulating Glass Unit Manufacturer.

WIND LOAD CHARTS

Mullions are designed for deflection limitations in accordance with AAMA TIR-A11 of L/175 up to 13'-6" and L/240 +1/4" above 13'-6". These curves are for mullions WITH HORIZONTALS and are based on engineering calculations for stress and deflection. Allowable wind load stress for ALUMINUM 15,152 psi (104 MPa), STEEL 30,000 psi (207 MPa). Charted curves, in all cases are for the limiting value. Wind load charts contained herein are based upon nominal wind load utilized in allowable stress design. A conversion from Load Resistance Factor Design (LRFD) is provided. To convert ultimate wind loads to nominal loads, multiply ultimate wind loads by a factor of 0.6 per ASCE/SEI 7. A 4/3 increase in allowable stress has not been used to develop these curves. For special situations not covered by these curves, contact your Kawneer representative for additional information.

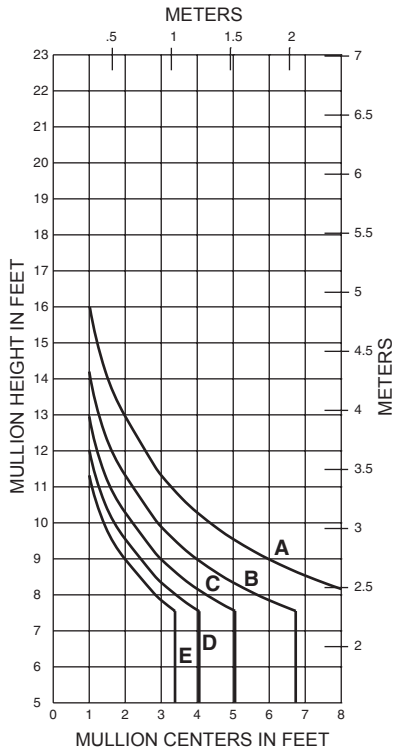
DEADLOAD CHARTS

Horizontal or deadload limitations are based upon 1/8" (3.2), maximum allowable deflection at the center of an intermediate horizontal member. The accompanying charts are calculated for 1" (25.4) thick insulating glass or 1/4" (6.4) thick glass supported on two setting blocks placed at the loading points shown.

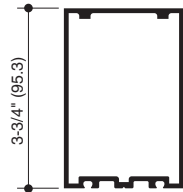
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SINGLE SPAN



	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

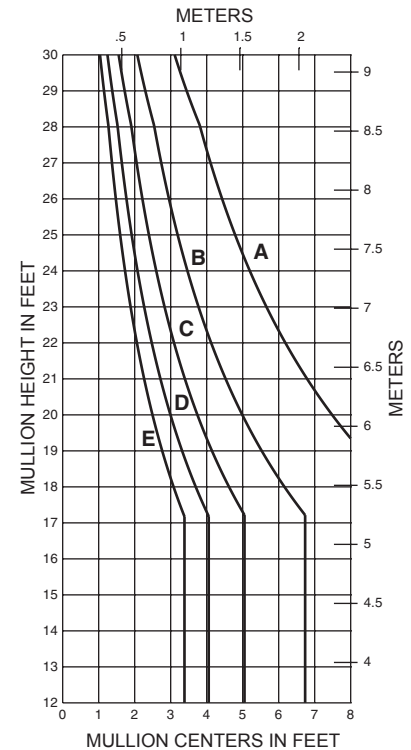


162025

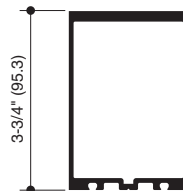
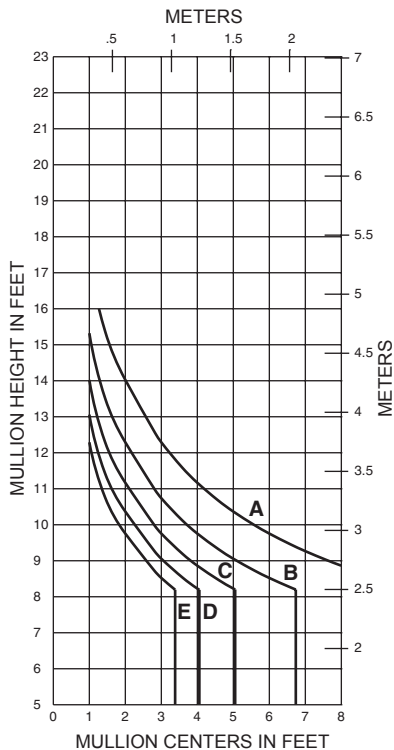
$I = 2.860 (119.04 \times 10^4)$
 $S = 1.482 (24.28 \times 10^3)$



TWIN SPAN



SINGLE SPAN

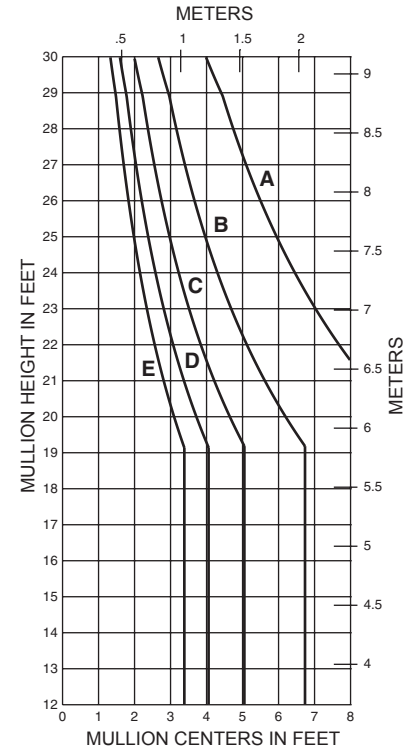


162026

$I = 3.660 (152.34 \times 10^4)$
 $S = 1.840 (30.15 \times 10^3)$



TWIN SPAN

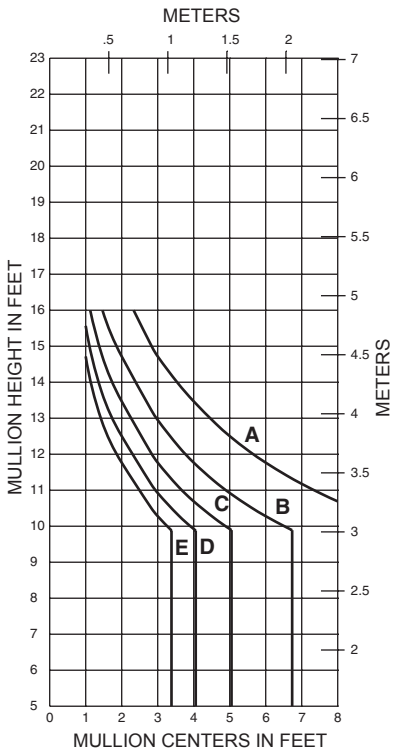


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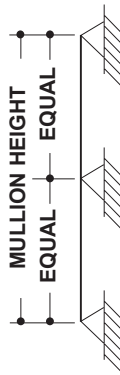
SINGLE SPAN



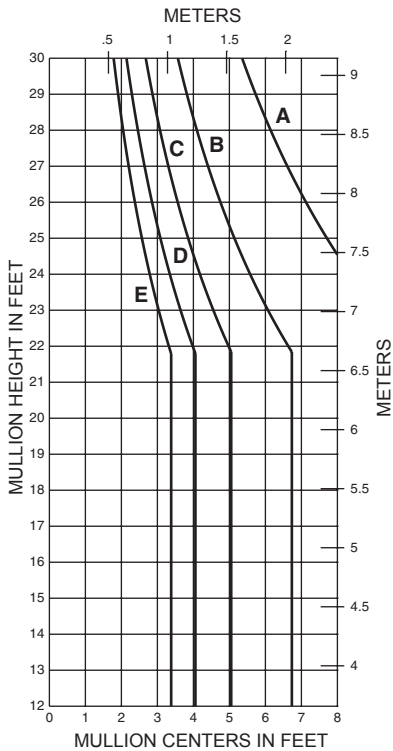
	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)



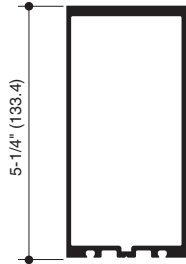
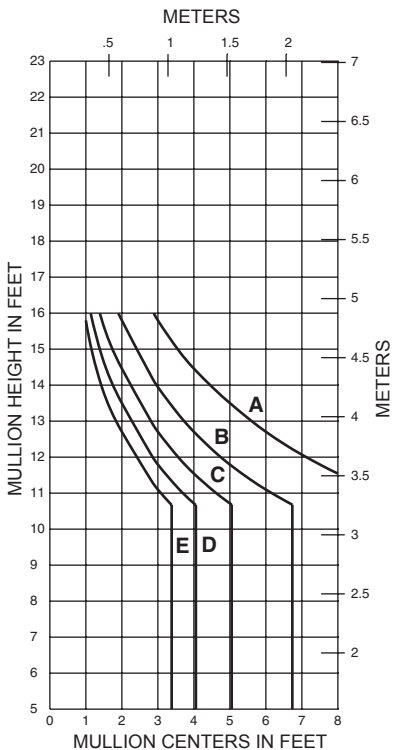
160207
I = 6.424 (267.38 x 10⁴)
S = 2.385 (39.08 x 10³)



TWIN SPAN



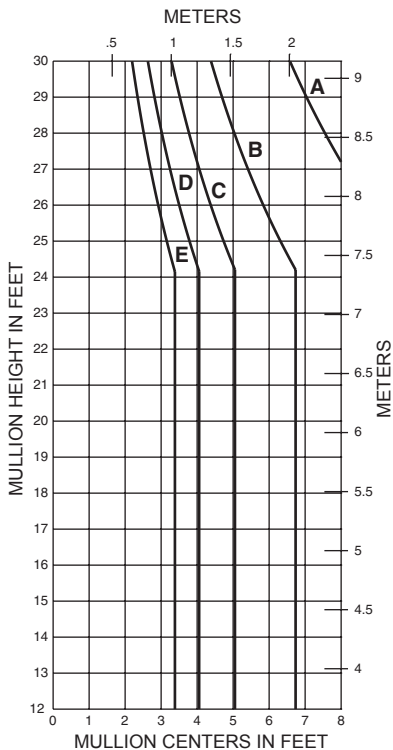
SINGLE SPAN



160208
I = 8.088 (336.64 x 10⁴)
S = 2.930 (48.01 x 10³)



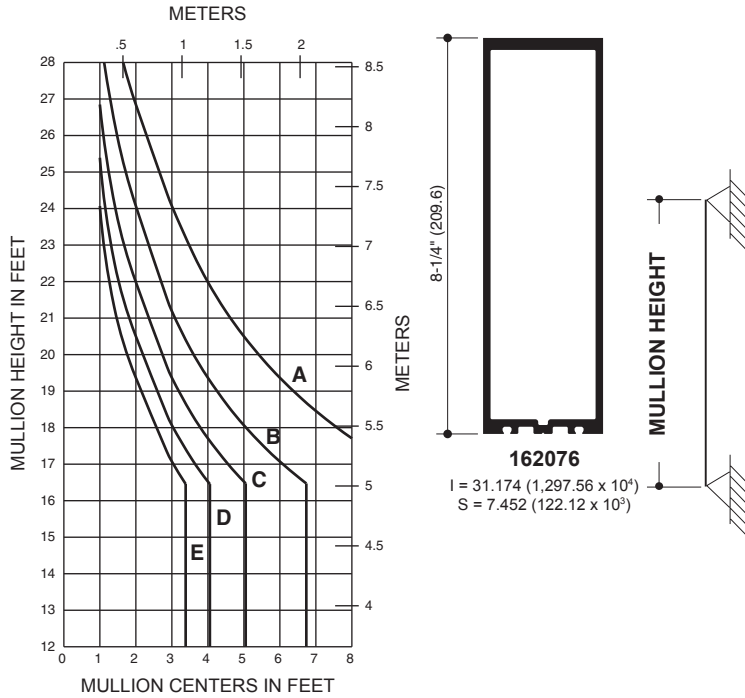
TWIN SPAN



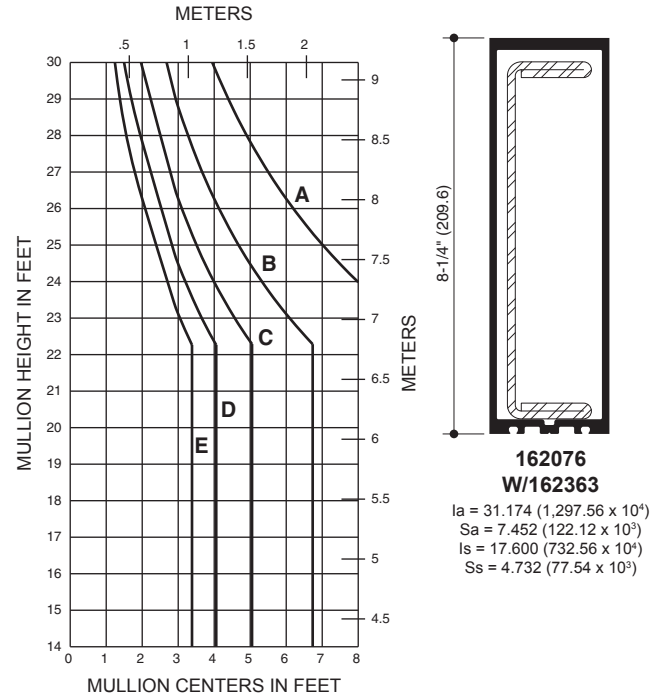
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SINGLE SPAN

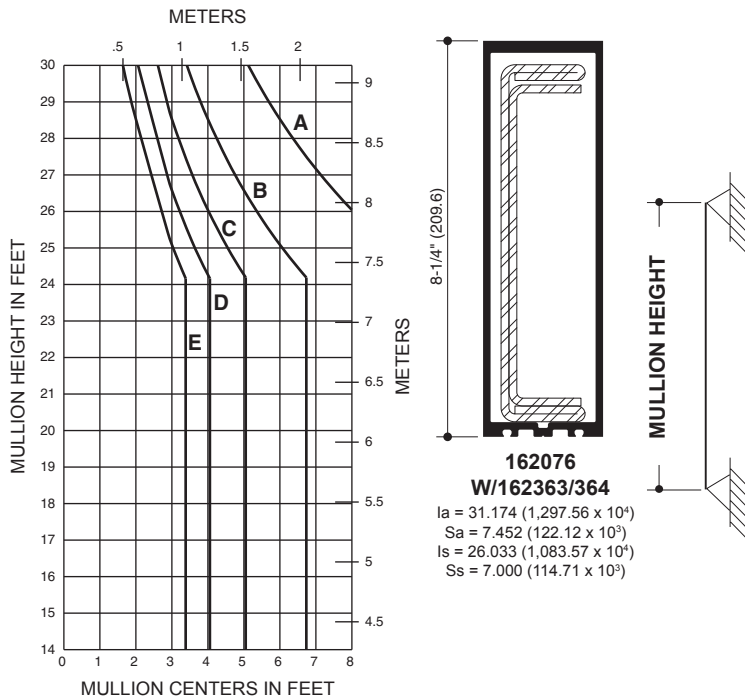


SINGLE SPAN

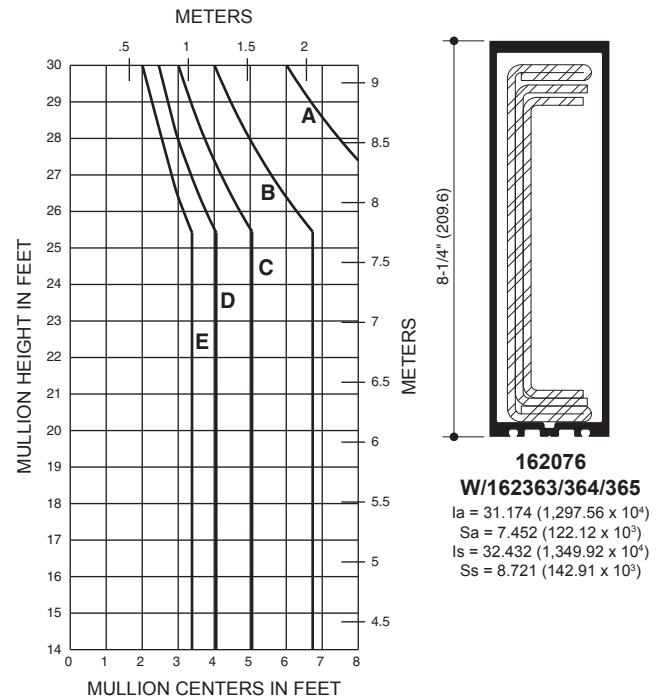


	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

SINGLE SPAN



SINGLE SPAN



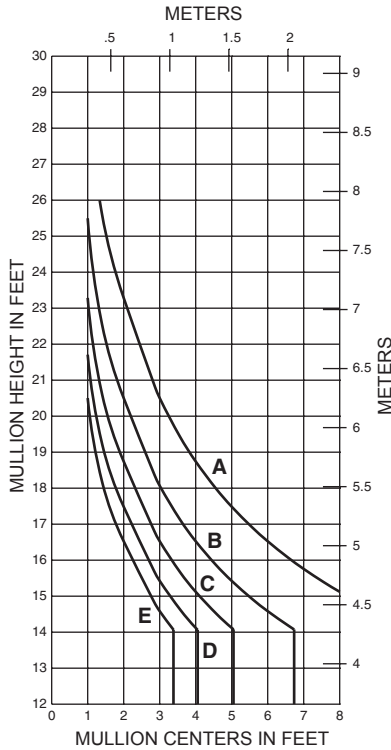
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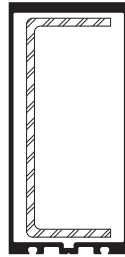
© Kawneer Company, Inc., 2014

SINGLE SPAN

162028 W/162300

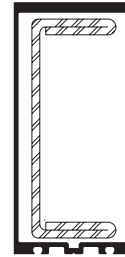


	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)



162028 with 162300

$I_a = 8.088 (336.64 \times 10^4)$
 $S_a = 2.930 (48.01 \times 10^3)$
 $I_s = 3.805 (158.37 \times 10^4)$
 $S_s = 1.669 (27.35 \times 10^3)$

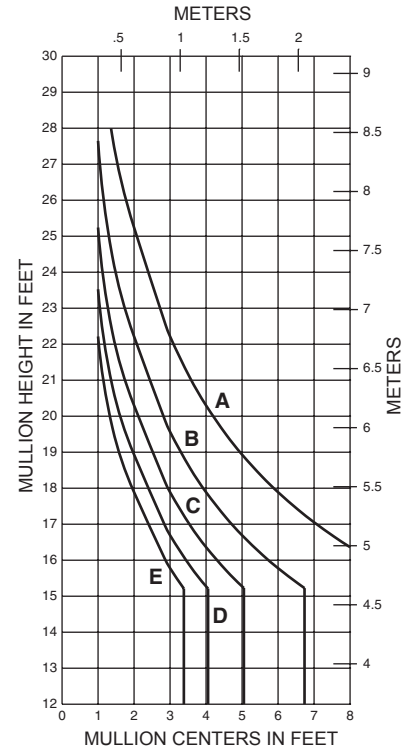


162028 with 162301

$I_a = 8.088 (336.64 \times 10^4)$
 $S_a = 2.930 (48.01 \times 10^3)$
 $I_s = 5.684 (236.59 \times 10^4)$
 $S_s = 2.493 (40.85 \times 10^3)$

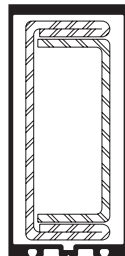
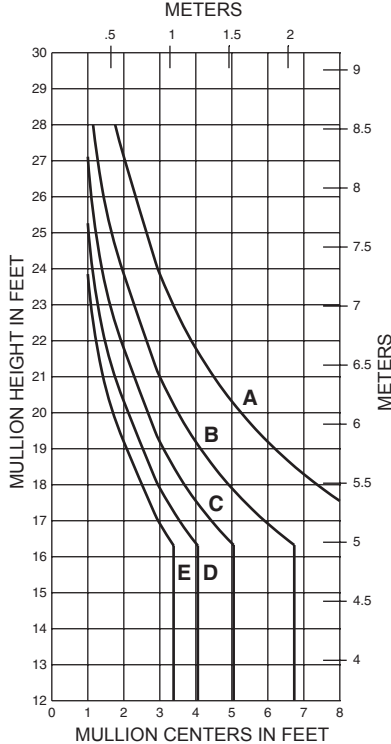
SINGLE SPAN

162028 W/162301



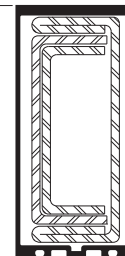
SINGLE SPAN

162028 W/162301/302



162028 with 162301/302

$I_a = 8.088 (336.64 \times 10^4)$
 $S_a = 2.930 (48.01 \times 10^3)$
 $I_s = 7.893 (328.53 \times 10^4)$
 $S_s = 3.462 (56.73 \times 10^3)$

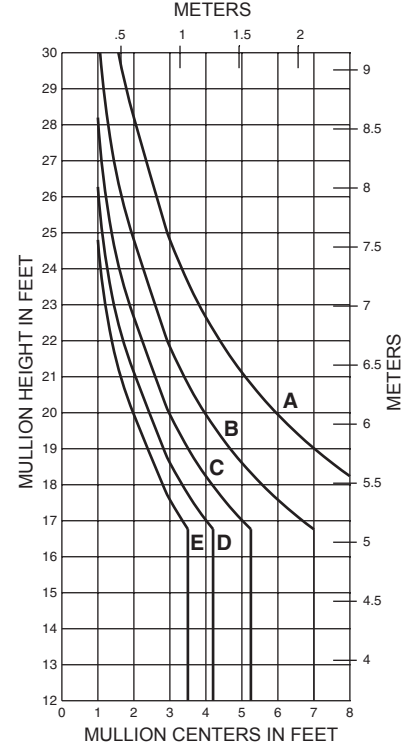


162028 with 162301/302/303

$I_a = 8.088 (336.64 \times 10^4)$
 $S_a = 2.930 (48.01 \times 10^3)$
 $I_s = 9.347 (389.05 \times 10^4)$
 $S_s = 4.100 (67.19 \times 10^3)$

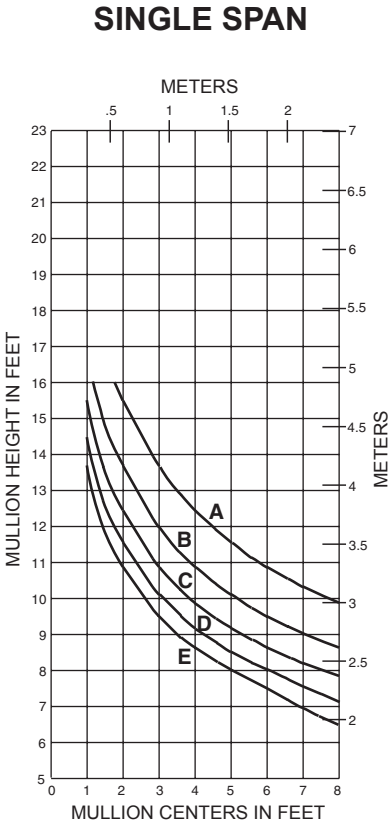
SINGLE SPAN

162028 W/162301/302/303

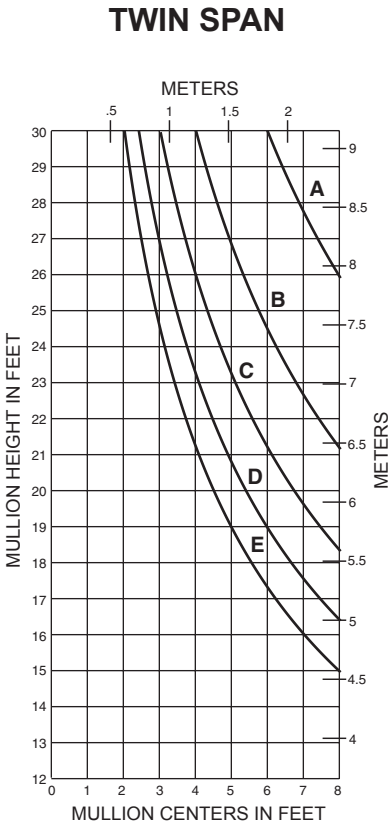
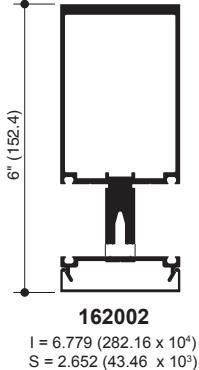
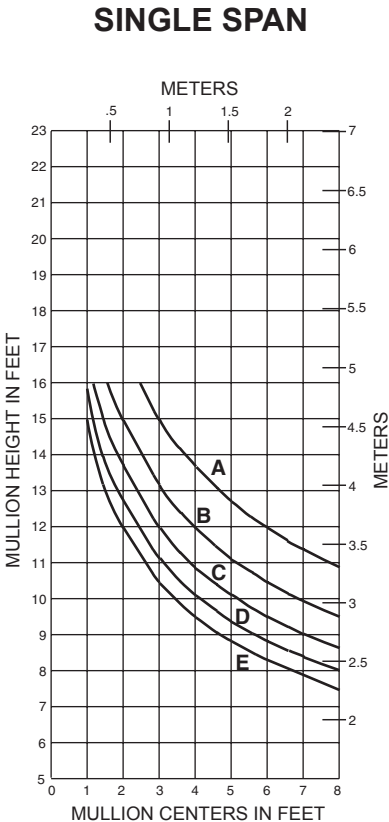
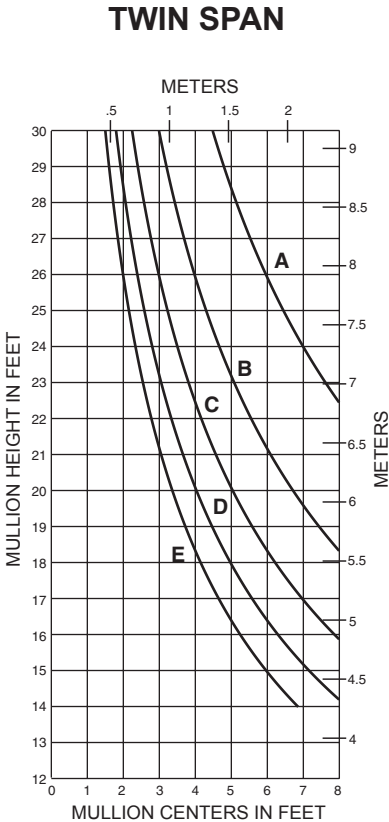


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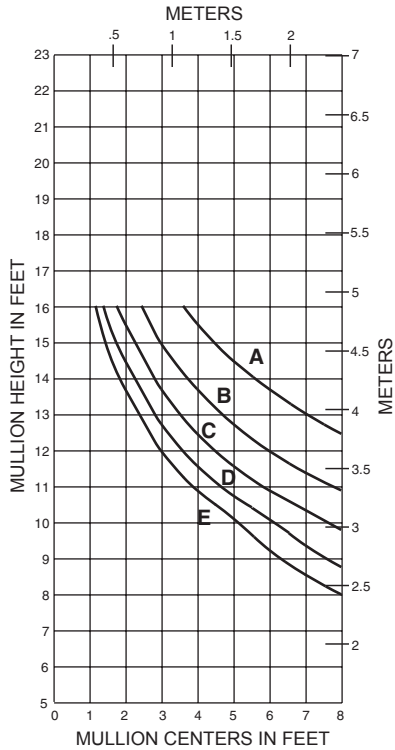
	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)



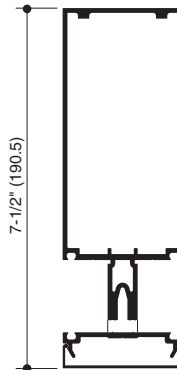
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SINGLE SPAN



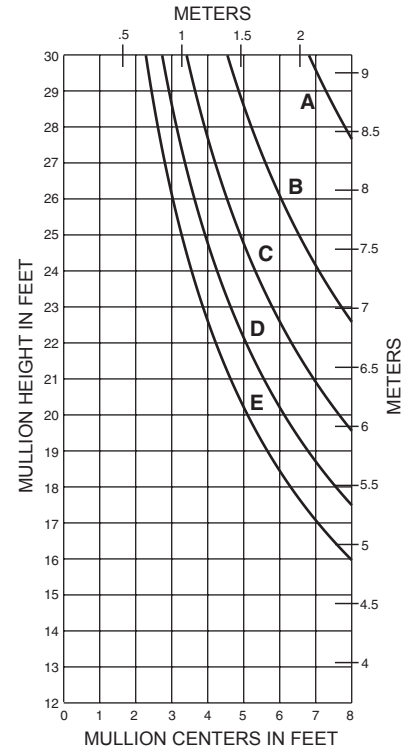
	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)



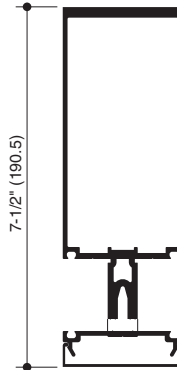
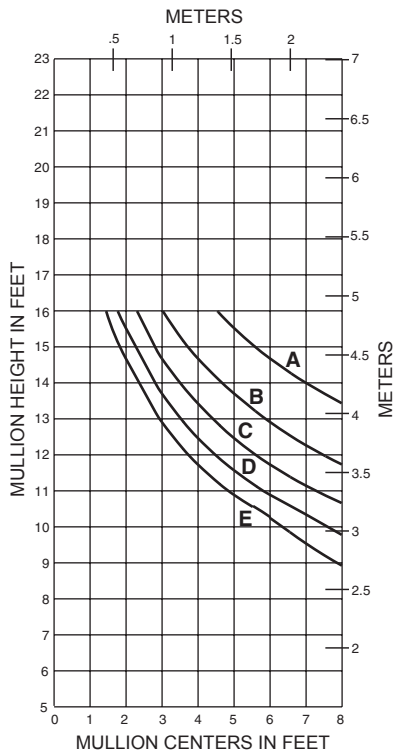
162003
 $I = 10.135 (421.85 \times 10^4)$
 $S = 3.027 (49.60 \times 10^3)$



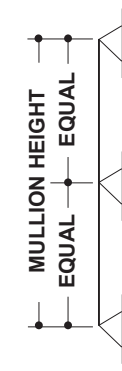
TWIN SPAN



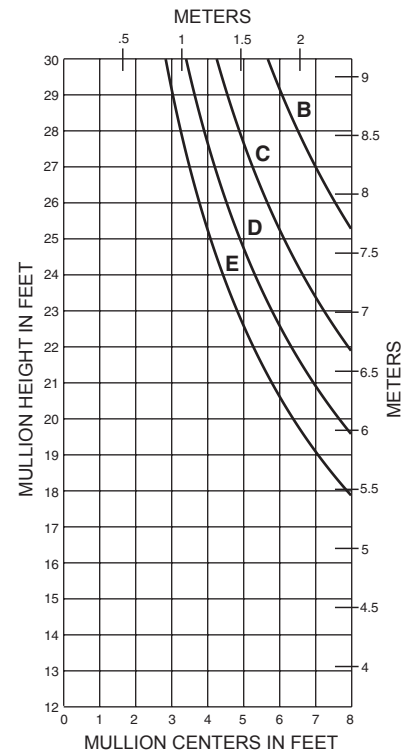
SINGLE SPAN



162004
 $I = 12.736 (530.11 \times 10^4)$
 $S = 3.791 (62.12 \times 10^3)$



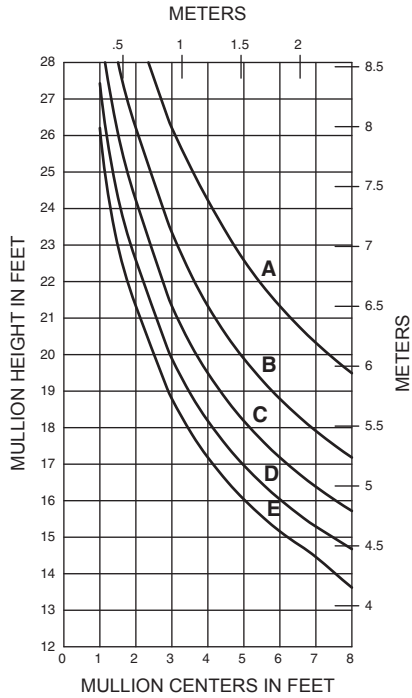
TWIN SPAN



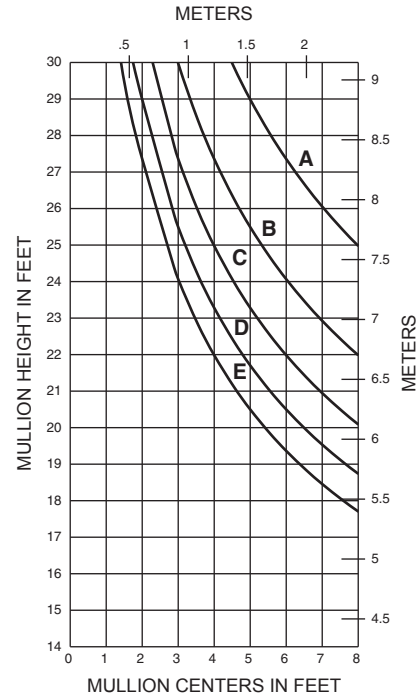
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SINGLE SPAN

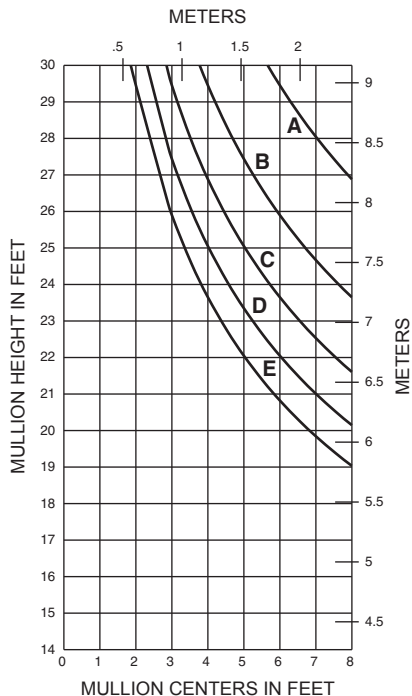


SINGLE SPAN

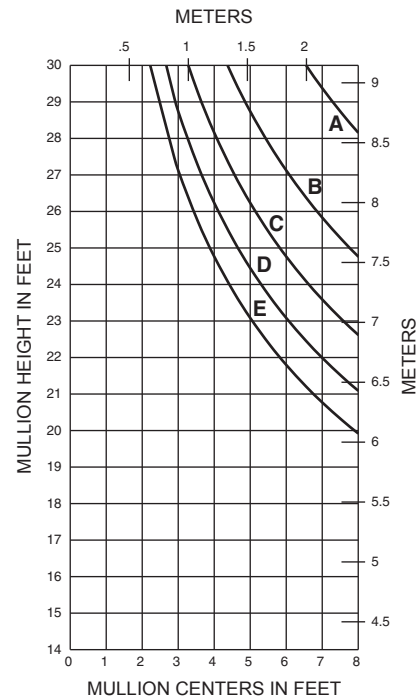


	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

SINGLE SPAN



SINGLE SPAN



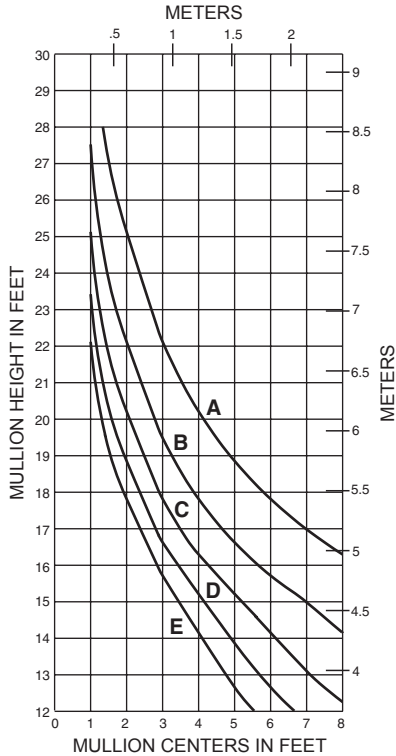
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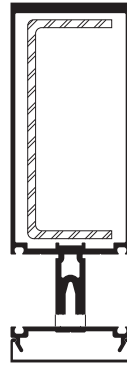
© Kawneer Company, Inc., 2014

SINGLE SPAN

162004 W/162300

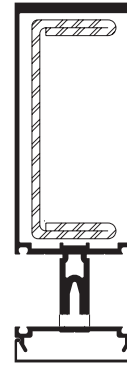


	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)



162004
with 162300

la = 12.736 (530.11 x 10⁴)
Sa = 3.791 (62.12 x 10³)
Is = 3.805 (158.37 x 10⁴)
Ss = 1.669 (27.35 x 10³)

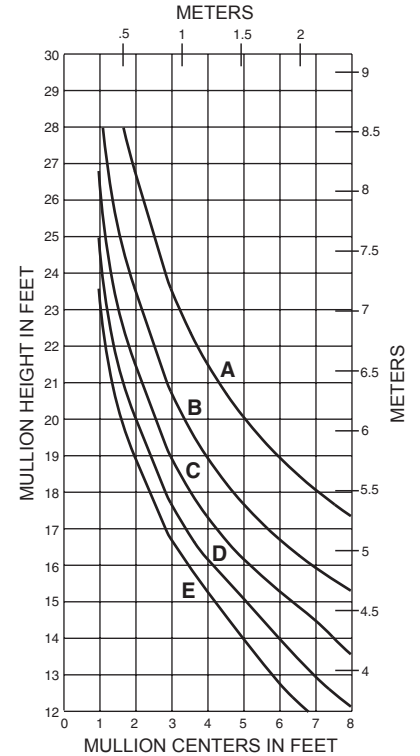


162004
with 162301

la = 12.736 (530.11 x 10⁴)
Sa = 3.791 (62.12 x 10³)
Is = 5.684 (236.59 x 10⁴)
Ss = 2.493 (40.85 x 10³)

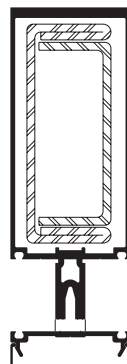
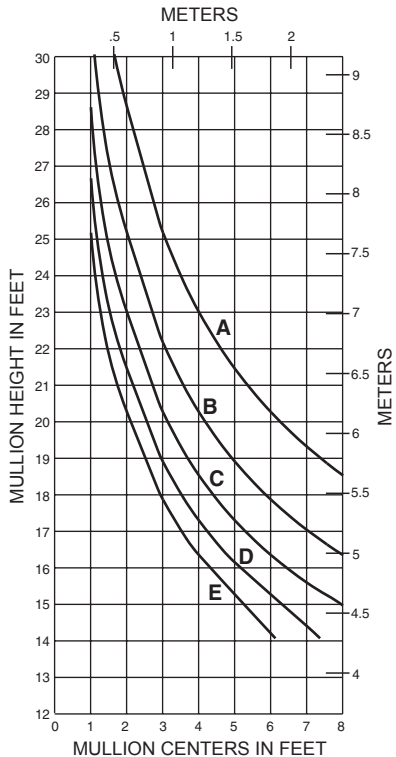
SINGLE SPAN

162004 W/162301



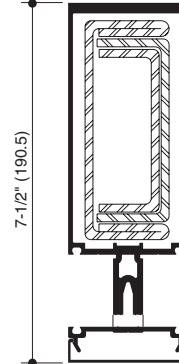
SINGLE SPAN

162004 W/162301/302



162004
with 162301/302

la = 12.736 (530.11 x 10⁴)
Sa = 3.791 (62.12 x 10³)
Is = 7.893 (328.53 x 10⁴)
Ss = 3.462 (56.73 x 10³)

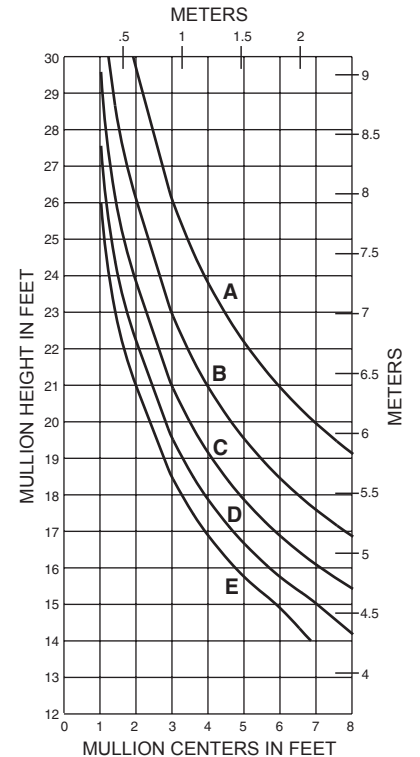


162004
with 162301/302/303

la = 12.736 (530.11 x 10⁴)
Sa = 3.791 (62.12 x 10³)
Is = 9.347 (389.05 x 10⁴)
Ss = 4.100 (67.19 x 10³)

SINGLE SPAN

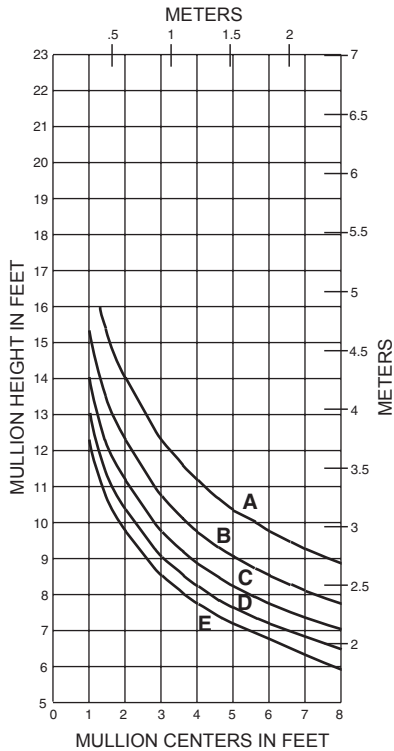
162004 W/162301/302/303



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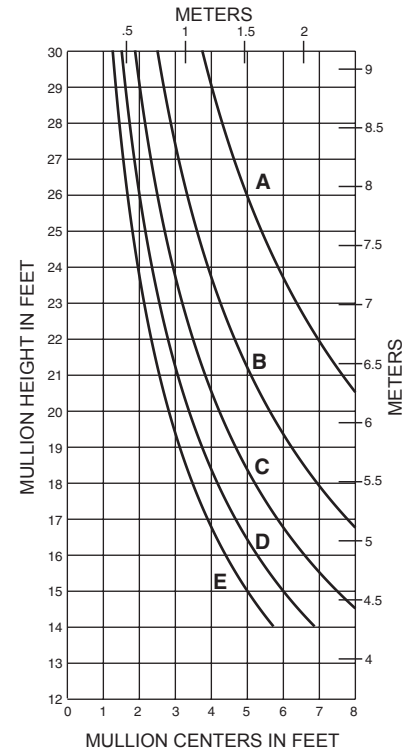
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SINGLE SPAN



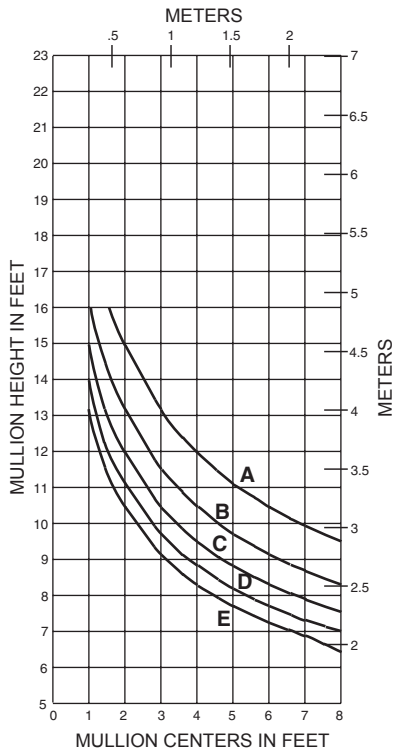
	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

TWIN SPAN

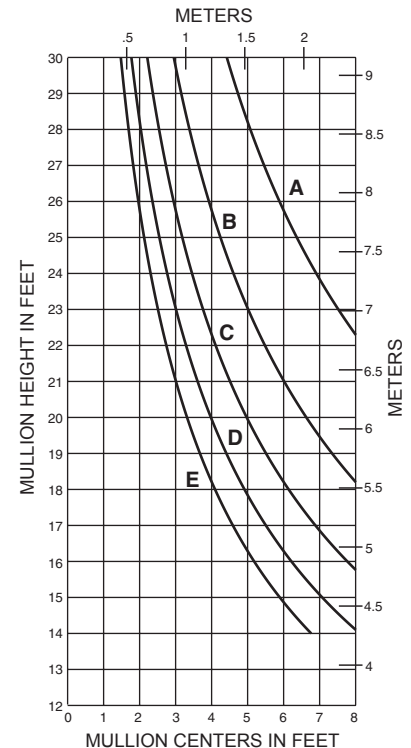


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SINGLE SPAN



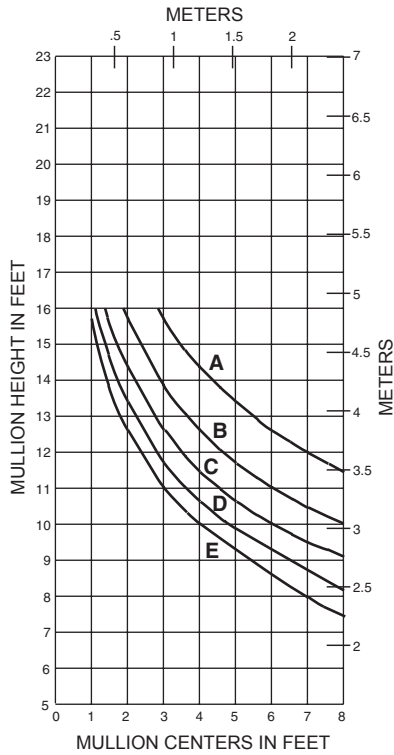
TWIN SPAN



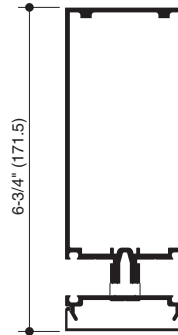
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SINGLE SPAN



	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

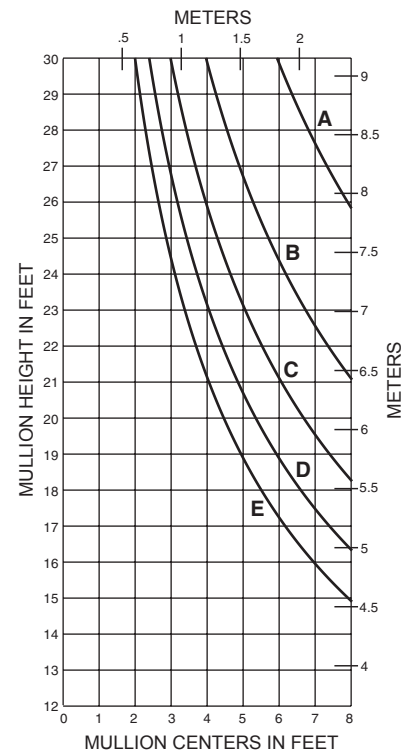


162015

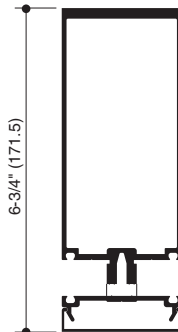
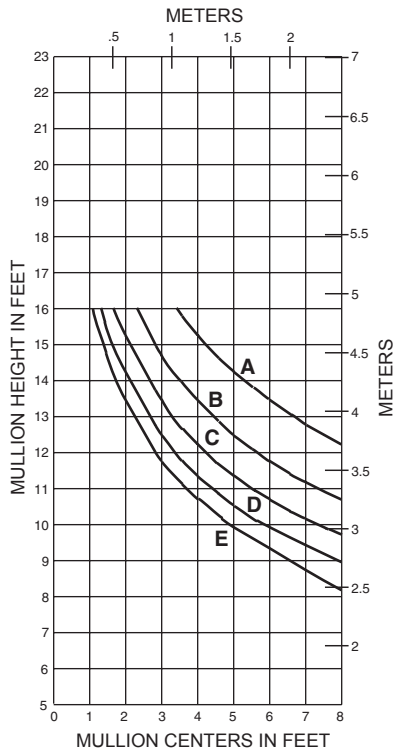
I = 7.915 (329.45 x 10⁶)
S = 2.635 (43.18 x 10³)



TWIN SPAN



SINGLE SPAN

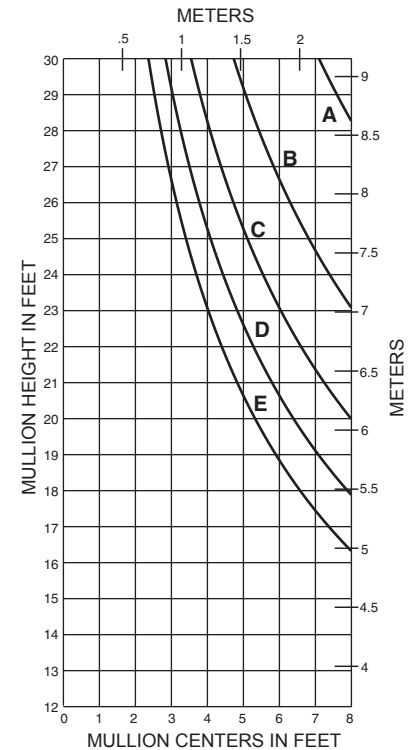


162016

I = 9.594 (399.33 x 10⁶)
S = 3.163 (51.83 x 10³)



TWIN SPAN

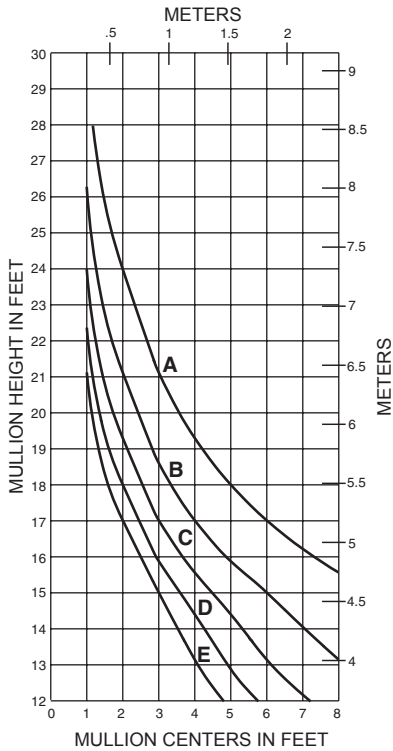


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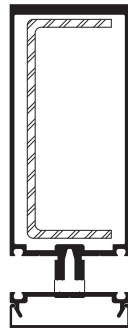
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SINGLE SPAN

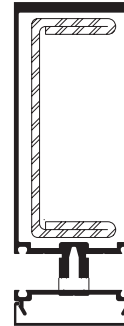
162016 W/162300



	Allowable Stress Design Load	LRFD Ultimate Design Load
A =	20 PSF (960)	33 PSF (1580)
B =	30 PSF (1440)	50 PSF (2400)
C =	40 PSF (1920)	67 PSF (3200)
D =	50 PSF (2400)	83 PSF (4000)
E =	60 PSF (2880)	100 PSF (4790)

162016
with 162300

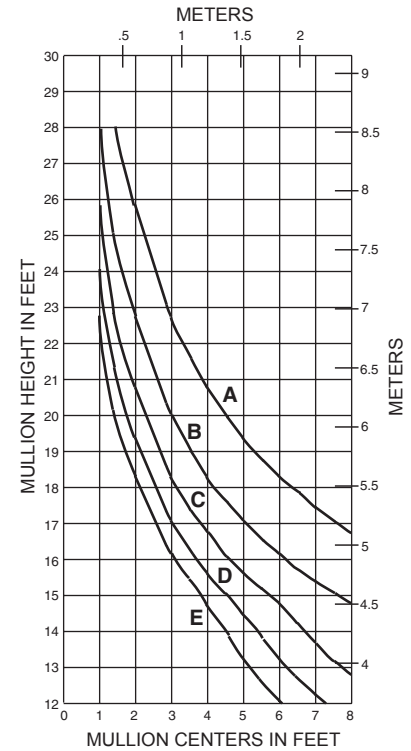
$I_a = 9.594 (399.33 \times 10^4)$
 $S_a = 3.163 (51.83 \times 10^3)$
 $I_s = 3.805 (158.37 \times 10^4)$
 $S_s = 1.669 (27.35 \times 10^3)$

162016
with 162301

$I_a = 9.594 (399.33 \times 10^4)$
 $S_a = 3.163 (51.83 \times 10^3)$
 $I_s = 5.684 (236.59 \times 10^4)$
 $S_s = 2.493 (40.85 \times 10^3)$

SINGLE SPAN

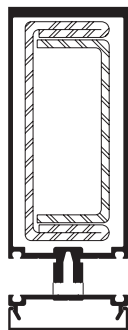
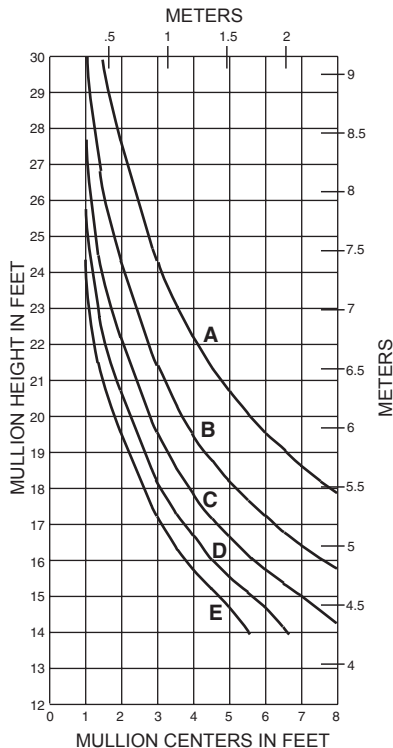
162016 W/162301



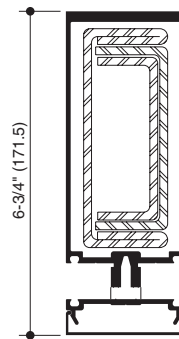
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SINGLE SPAN

162016 W/162301/302

162016
with 162301/302

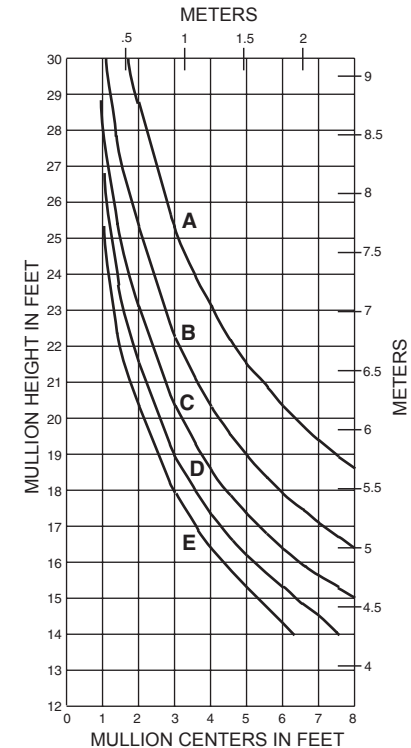
$I_a = 9.594 (399.33 \times 10^4)$
 $S_a = 3.163 (51.83 \times 10^3)$
 $I_s = 7.893 (328.53 \times 10^4)$
 $S_s = 3.462 (56.73 \times 10^3)$

162016
with 162301/302/303

$I_a = 9.594 (399.33 \times 10^4)$
 $S_a = 3.163 (51.83 \times 10^3)$
 $I_s = 9.347 (389.05 \times 10^4)$
 $S_s = 4.100 (67.19 \times 10^3)$

SINGLE SPAN

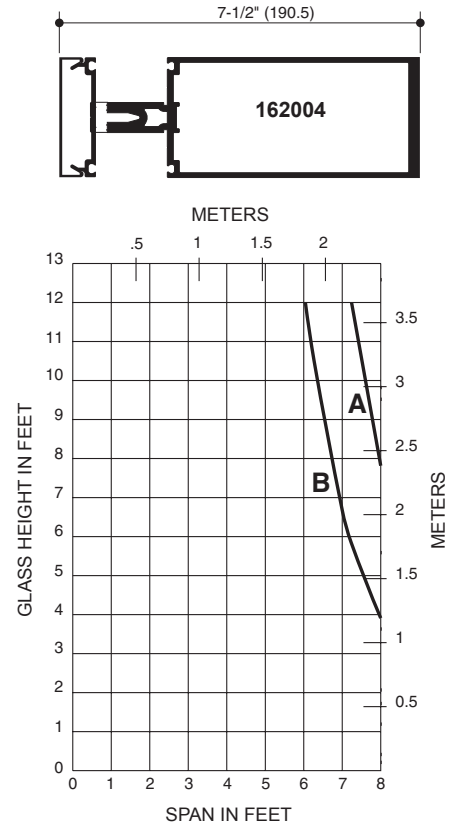
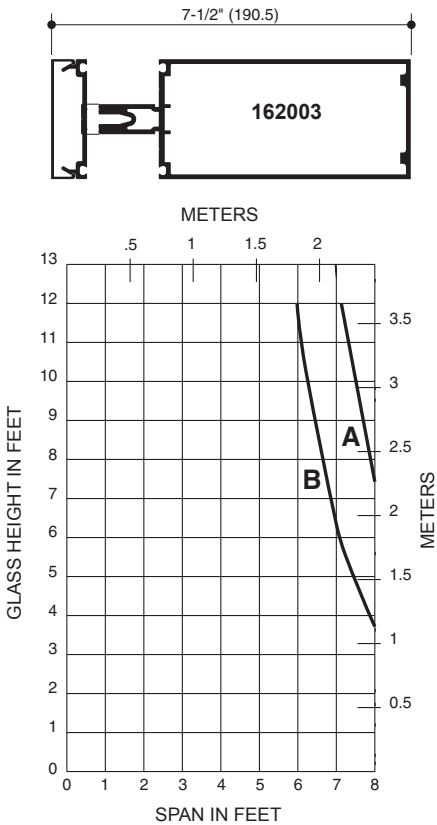
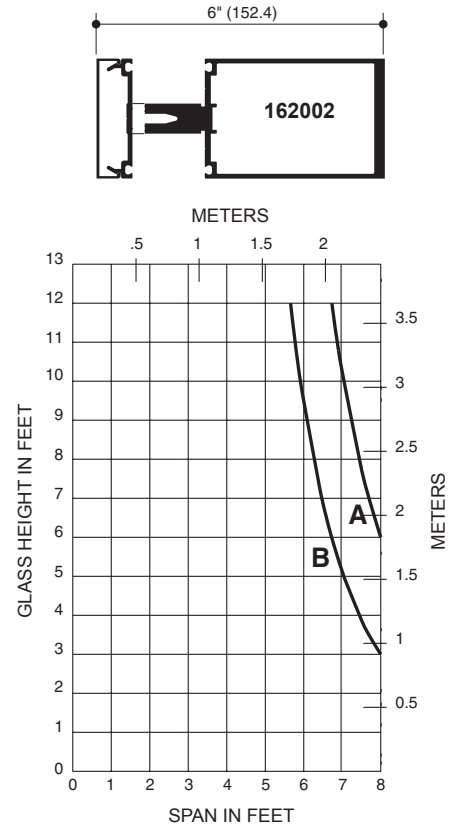
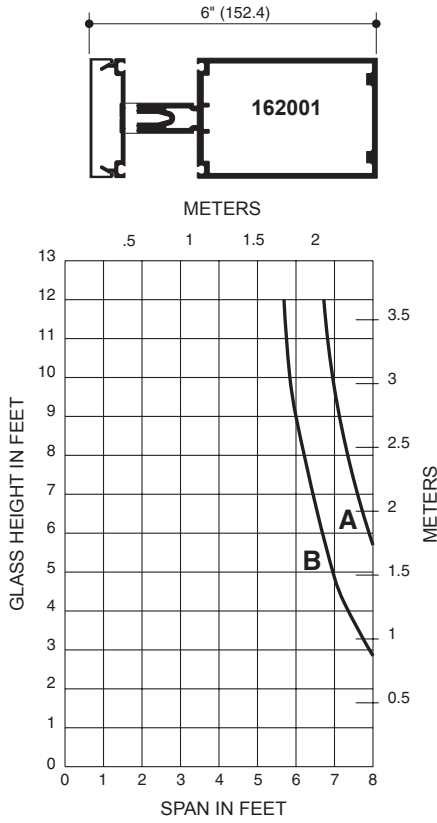
162016 W/162301/302/303



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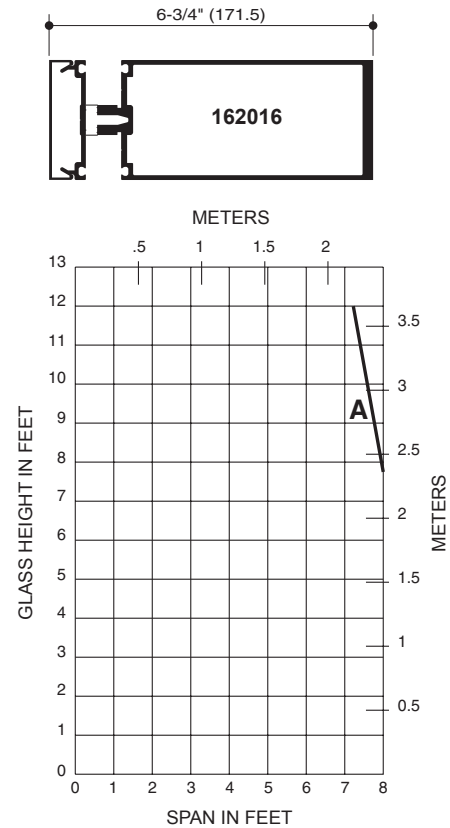
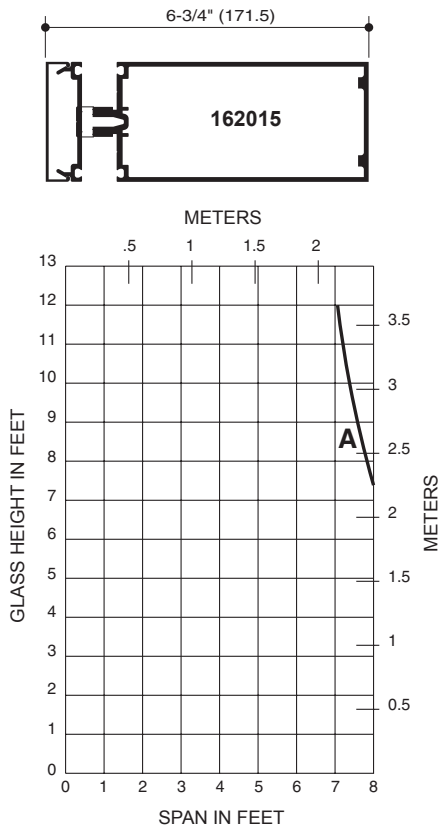
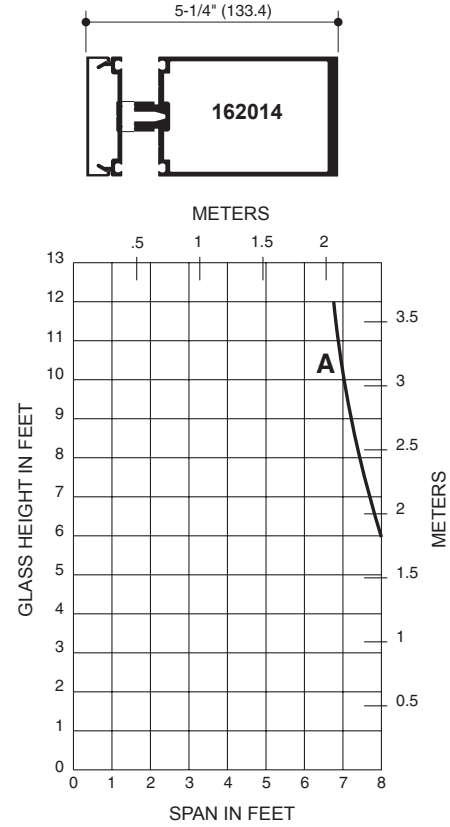
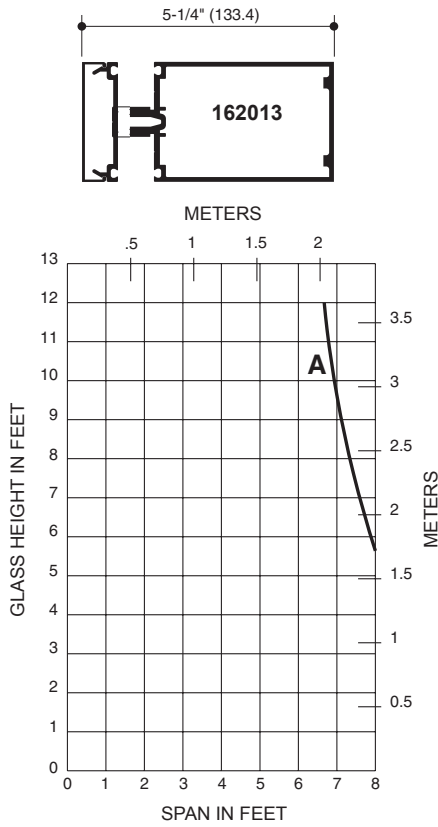
A - 1/4" GLASS (1/4 POINT LOADING)
B - 1" GLASS (1/4 POINT LOADING)



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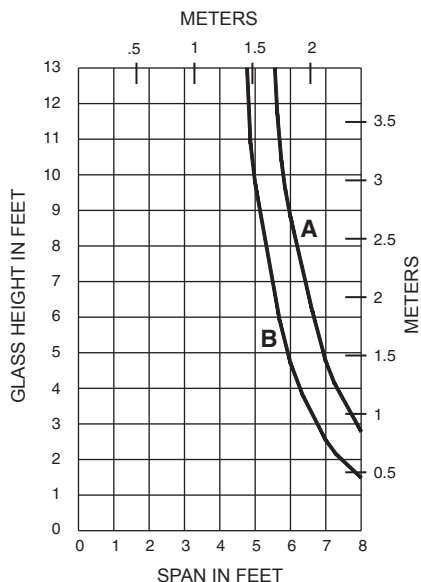
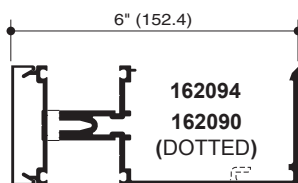
A - 1/4" GLASS (1/4 POINT LOADING)



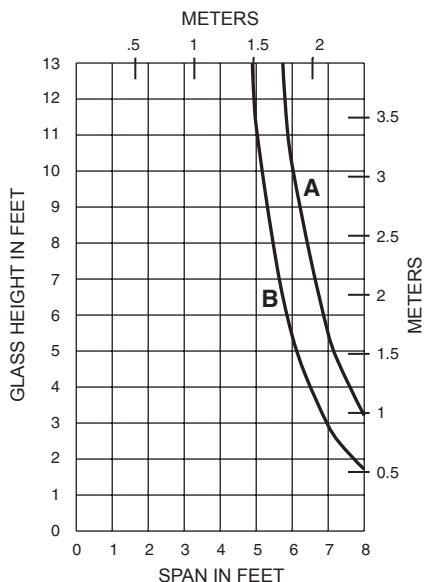
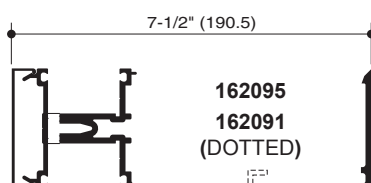
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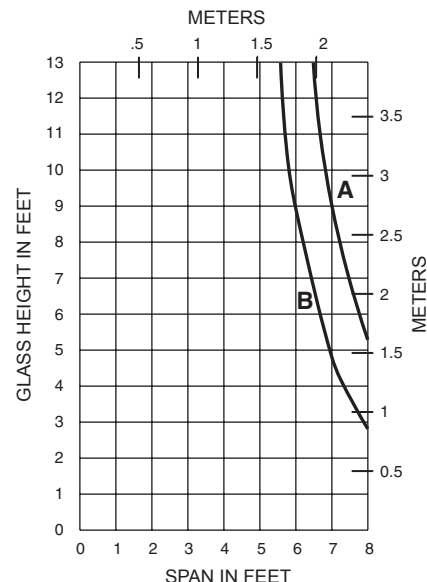
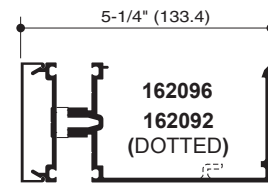
A - 1" GLASS (1/8 POINT LOADING)
B - 1" GLASS (1/4 POINT LOADING)



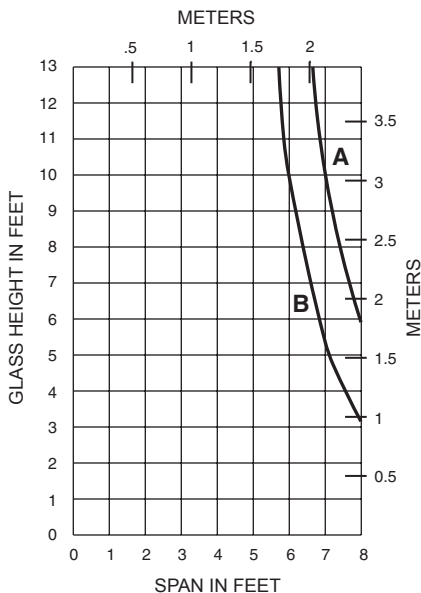
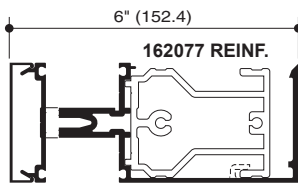
A - 1" GLASS (1/8 POINT LOADING)
B - 1" GLASS (1/4 POINT LOADING)



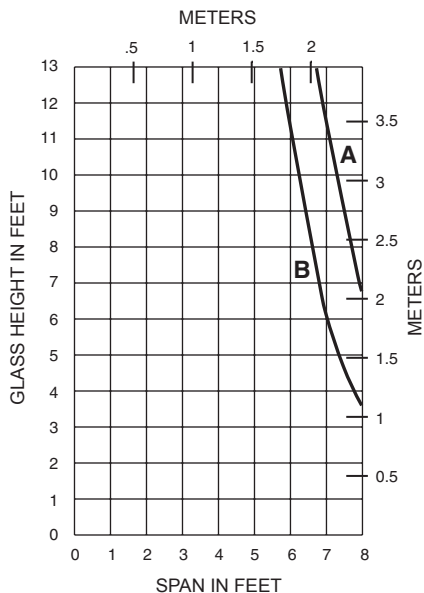
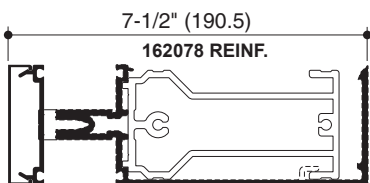
A - 1/4" GLASS (1/8 POINT LOADING)
B - 1/4" GLASS (1/4 POINT LOADING)



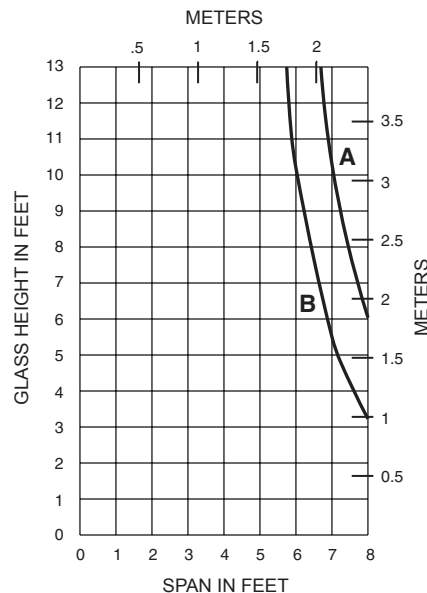
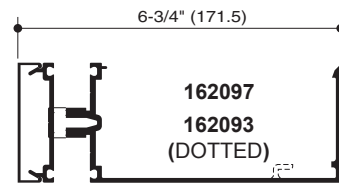
A - 1" GLASS (1/8 POINT LOADING)
B - 1" GLASS (1/4 POINT LOADING)



A - 1" GLASS (1/8 POINT LOADING)
B - 1" GLASS (1/4 POINT LOADING)



A - 1/4" GLASS (1/8 POINT LOADING)
B - 1/4" GLASS (1/4 POINT LOADING)

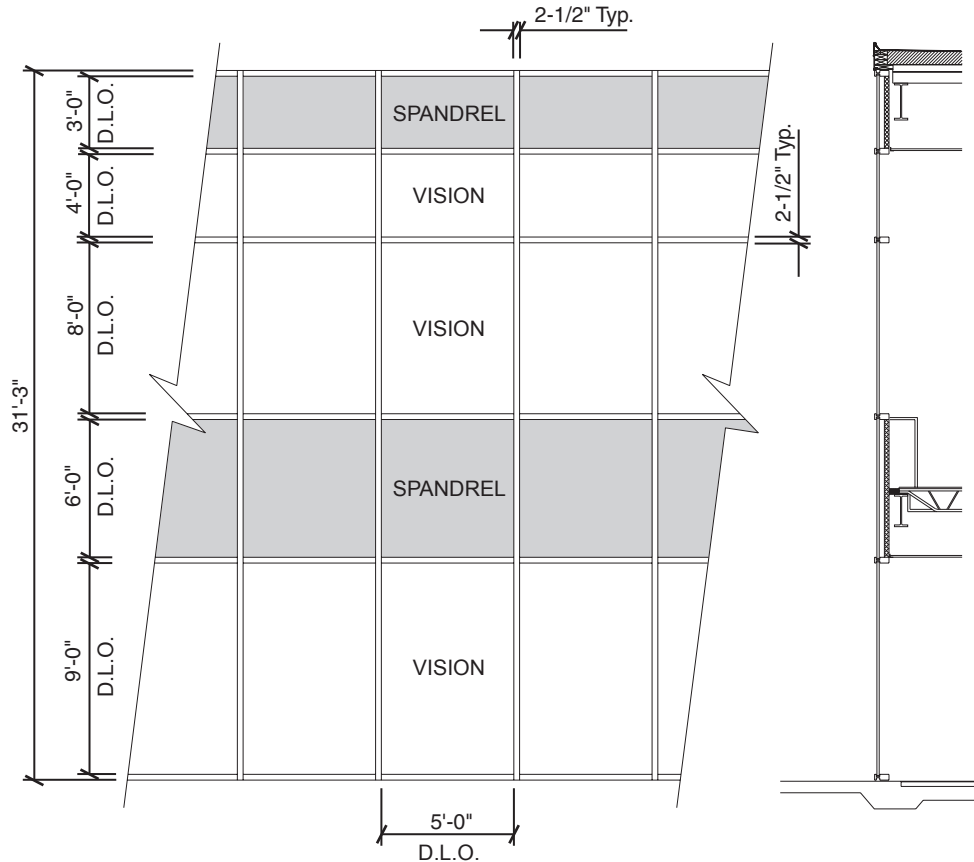


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Generic Project Specific U-factor Example Calculation
(Percent of Glass will vary on specific products depending on sitelines)
 (Based on single bay of Curtain Wall/Window Wall)



Vision Area

Example Glass U-factor	= 0.48 Btu/(ft ² · h · °F)
Vision Area	= 5(9 + 8 + 4) = 105.0 ft ²
Total Area (Vision)	= 5' 2-1/2" (9' 3-3/4" + 8' 2-1/2" + 4' 2-1/2") = 113.2 ft ²
Percentage of Vision Glass	= (Vision Area ÷ Total Area)100 = (105.0 ÷ 113.2)100 = 93%

Spandrel Area

Example Spandrel R-value	= 15 (ft ² · h · °F)/Btu
Spandrel Area	= 5(6 + 3) = 45.0 ft ²
Total Area (Spandrel)	= 5' 2-1/2" (6' 2-1/2" + 3' 3-3/4") = 49.6 ft ²
Percent of Spandrel	= (Spandrel Area ÷ Total Area)100 = (49.0 ÷ 49.6)100 = 91%

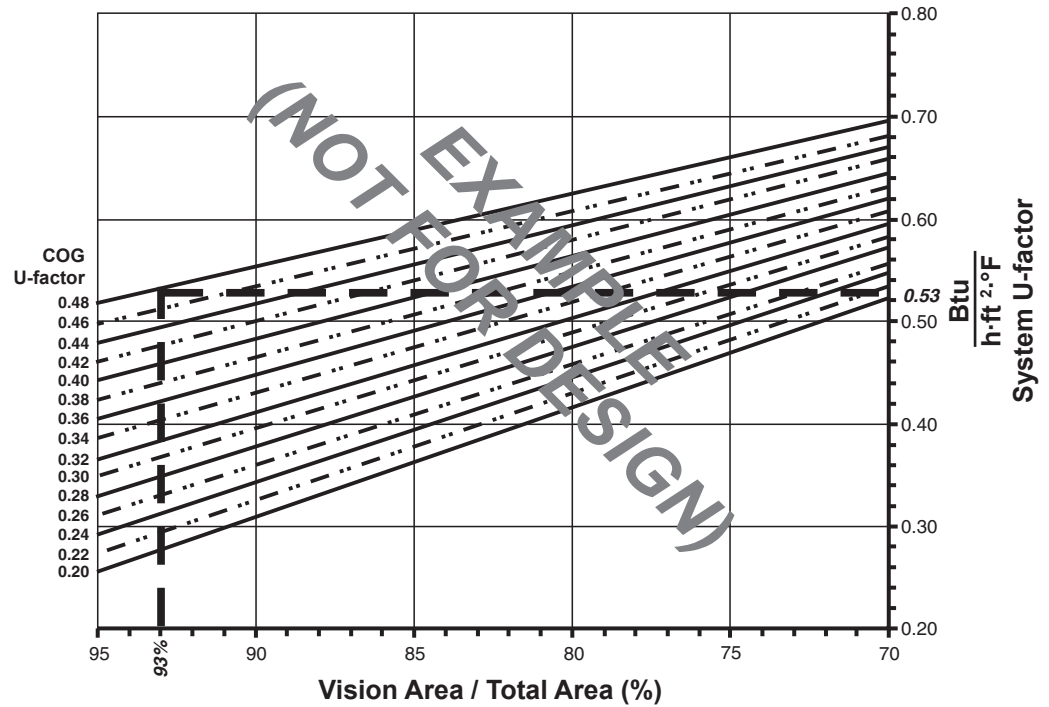
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Vision Area Chart

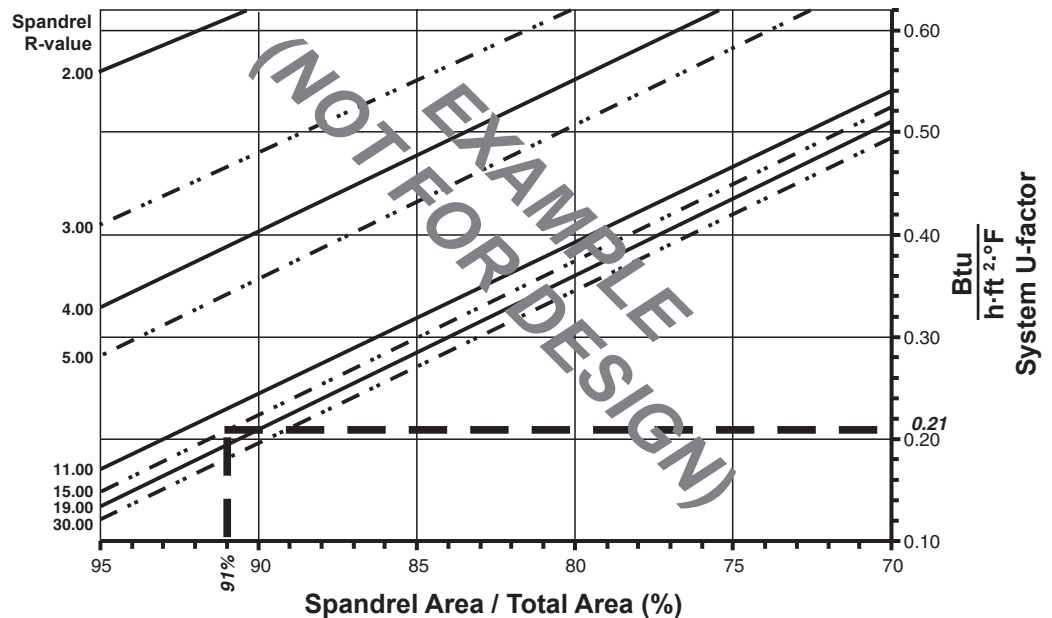
System U-factor vs Percent of Vision Area



Based on a single curtain wall bay of 93% vision glass and center of glass U-factor of 0.48, System U-factor is equal to 0.53 Btu/(h·ft²·°F)

Spandrel Area Chart

System U-factor vs Percent of Spandrel Area



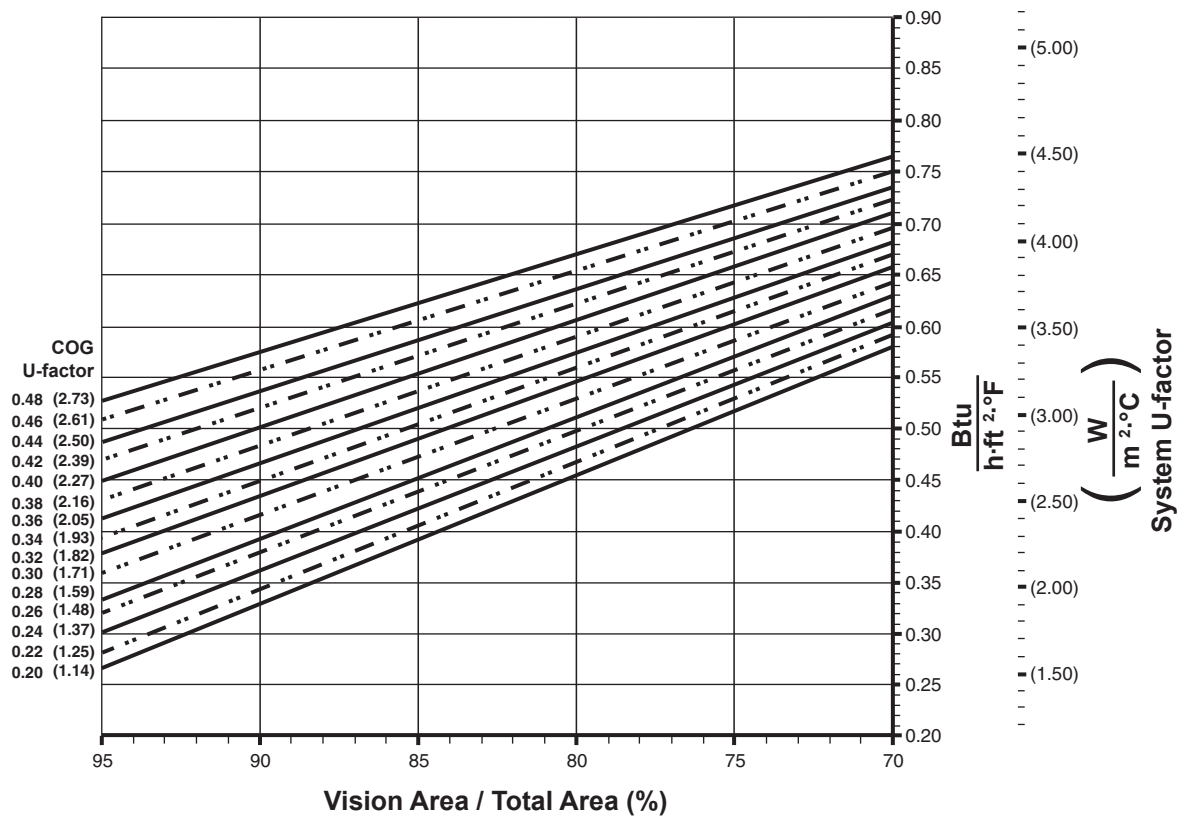
Based on a single curtain wall bay of 91% spandrel and center of spandrel R-value of 15, system U-factor is equal to 0.21 Btu/(h·ft²·°F)

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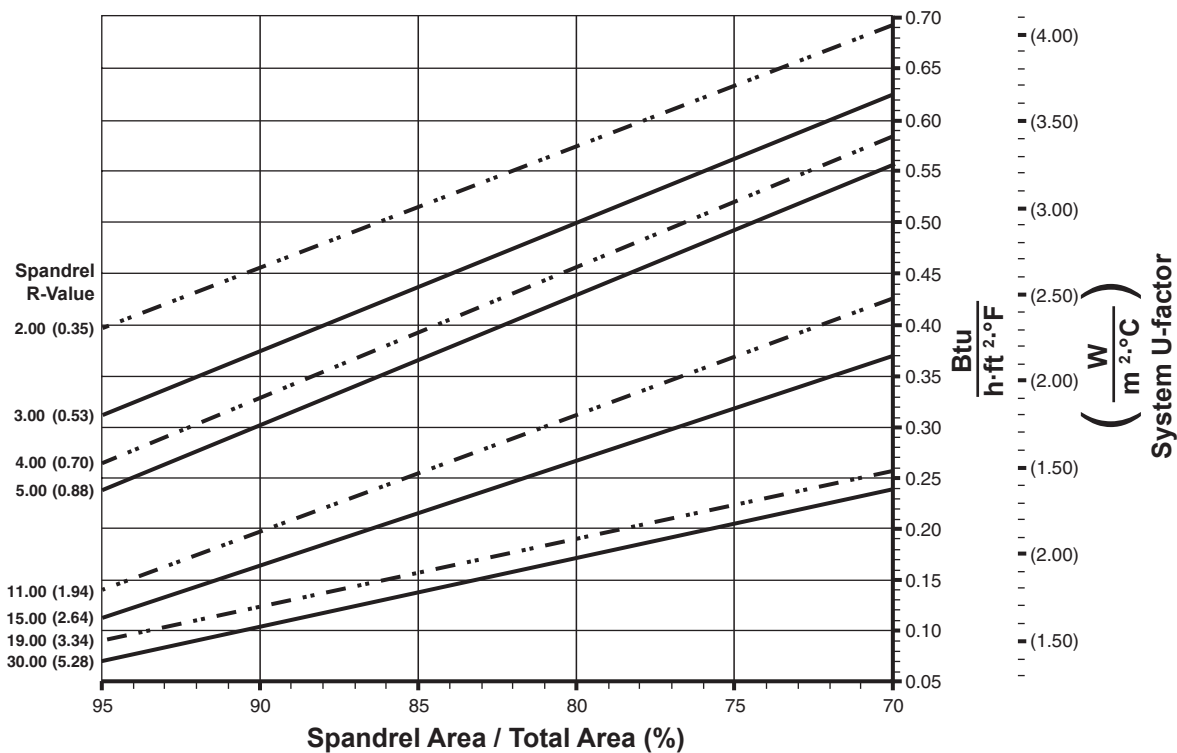
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Note:
Values in parentheses are metric.
COG=Center of Glass.
Charts are generated per AAMA 507.

System U-Factor for Vision Glass



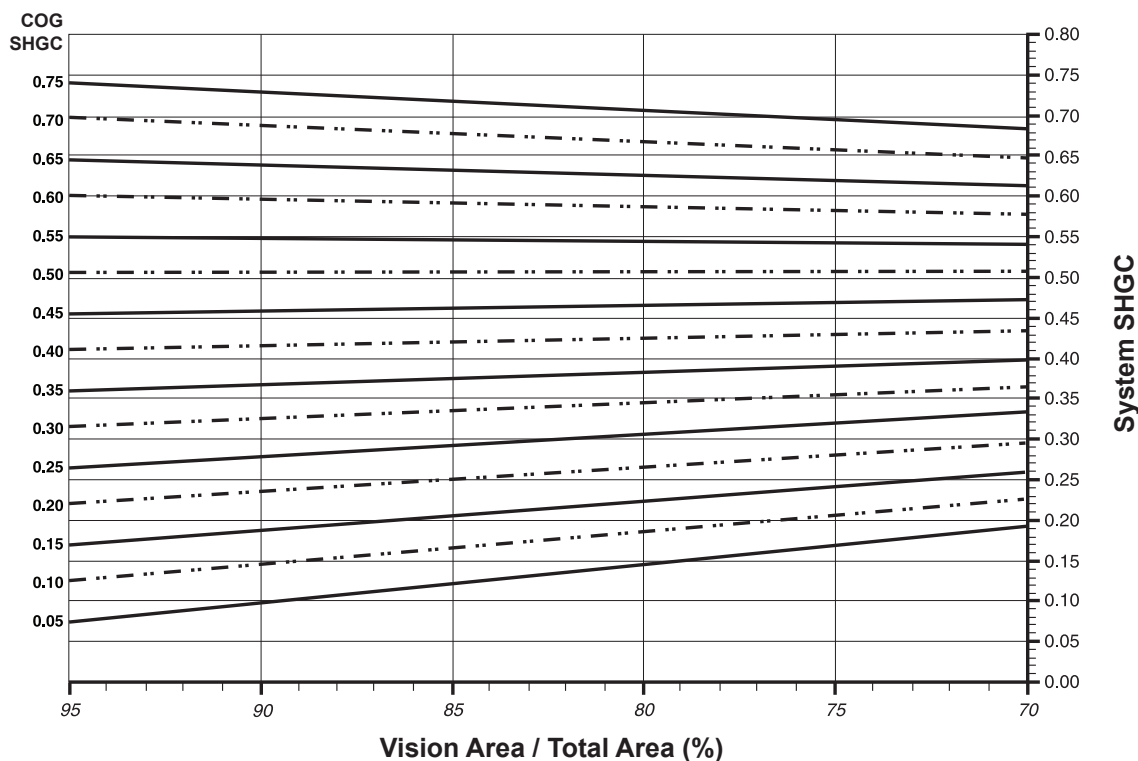
System U-Factors for Spandrel Glass



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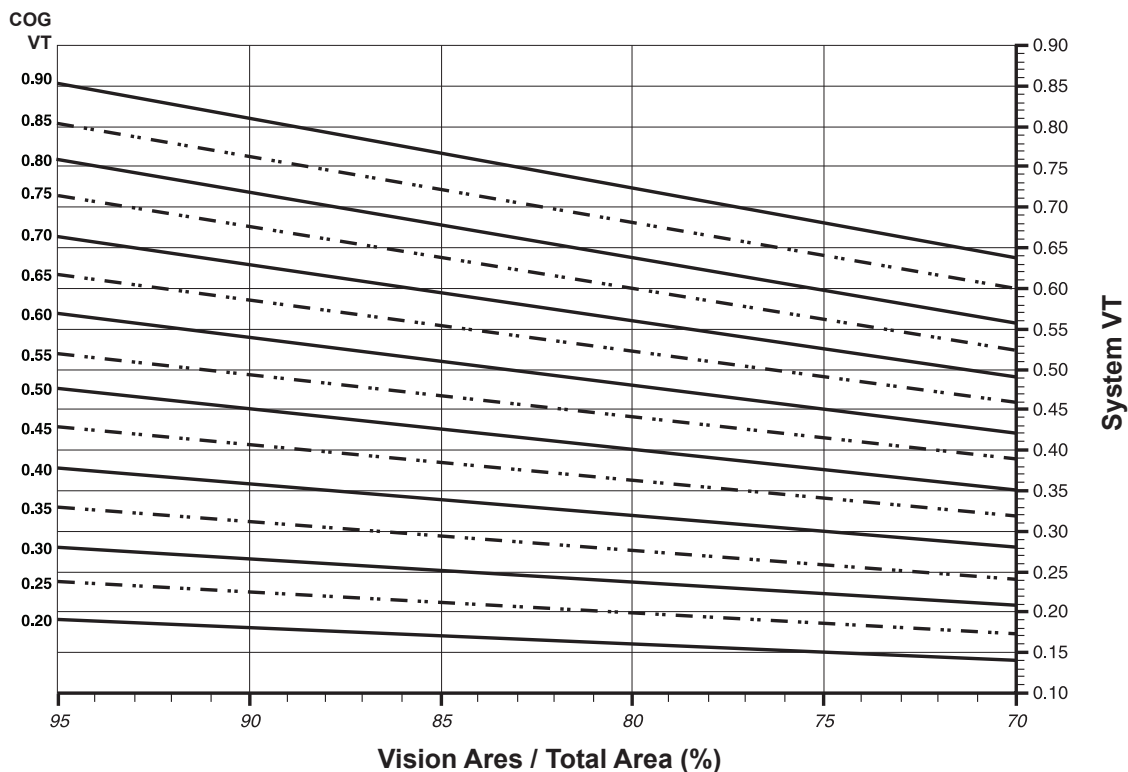
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System Solar Heat Gain Coefficient (SHGC) vs Percent of Vision Area



Charts are generated per AAMA 507.

System Visible Transmittance (VT) vs Percent of Vision Area



Charts are generated per AAMA 507.

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Thermal Transmittance¹ (BTU/hr • ft² • °F)

Glass U-Factor ³	Overall U-Factor ⁴
0.48	0.56
0.46	0.54
0.44	0.53
0.42	0.51
0.40	0.49
0.38	0.48
0.36	0.46
0.34	0.44
0.32	0.42
0.30	0.41
0.28	0.39
0.26	0.37
0.24	0.36
0.22	0.34
0.20	0.32

**1" GLAZING WITH
ALUMINUM PRESSURE PLATE**

NOTE: For glass values that are not listed, linear interpolation is permitted.

1. U-Factors are determined in accordance with NFRC 100.
2. SHGC and VT values are determined in accordance with NFRC 200.
3. Glass properties are based on center of glass values and are obtained from your glass supplier.
4. Overall U-Factor, SHGC, and VT Matricies are based on the standard NFRC specimen size of 2,000 mm wide by 2,000 mm high (78-3/4" by 78-3/4").

SHGC Matrix²

Glass SHGC ³	Overall SHGC ⁴
0.75	0.73
0.70	0.68
0.65	0.64
0.60	0.59
0.55	0.55
0.50	0.50
0.45	0.46
0.40	0.41
0.35	0.37
0.30	0.32
0.25	0.28
0.20	0.23
0.15	0.19
0.10	0.14
0.05	0.10

Visible Transmittance²

Glass VT ³	Overall VT ⁴
0.90	0.81
0.85	0.77
0.80	0.72
0.75	0.68
0.70	0.63
0.65	0.59
0.60	0.54
0.55	0.50
0.50	0.45
0.45	0.41
0.40	0.36
0.35	0.32
0.30	0.27
0.25	0.23
0.20	0.18

Laws and building and safety codes governing the design and use of glazed entrance, window, and curtain wall products vary widely. Kawneer does not control the selection of product configurations, operating hardware, or glazing materials, and assumes no responsibility therefor.

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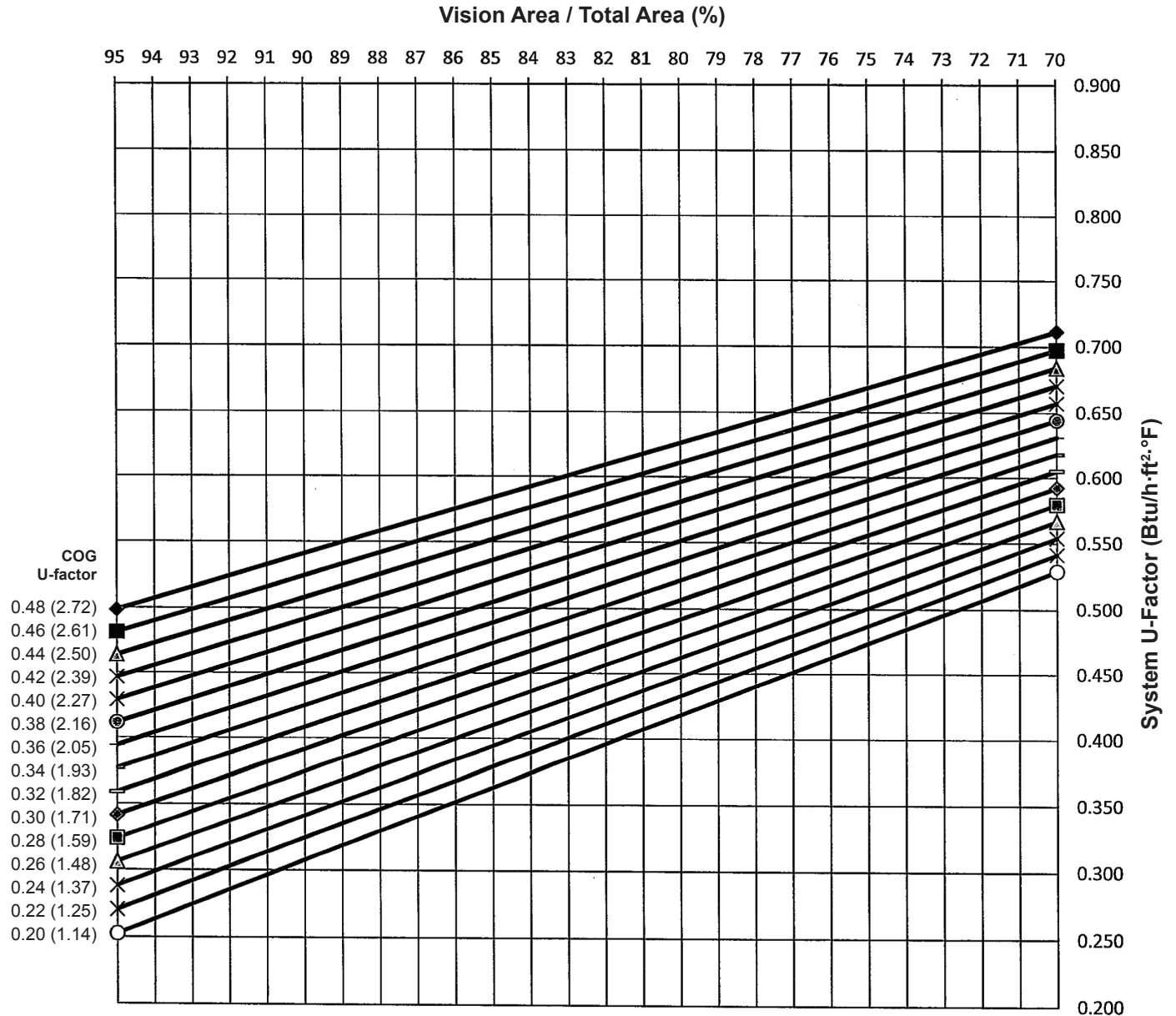
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Note:

Values in parentheses are metric.

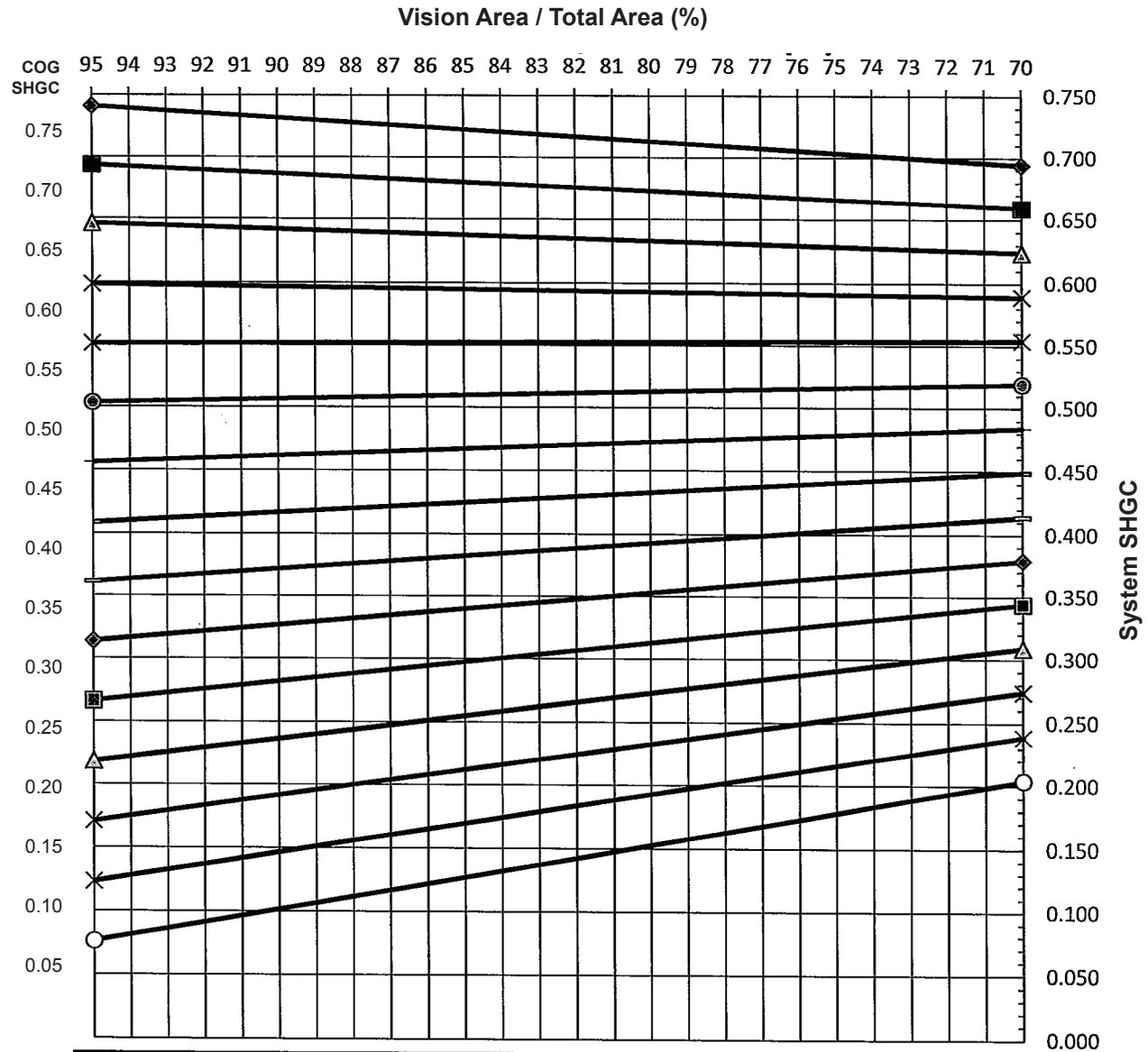
COG=Center of Glass.

Charts are generated per AAMA 507.

1" GLAZING WITH FIBERGLASS PRESSURE PLATE**System U-Factor for Vision Glass****Notes for System U-Factor, SHGC and VT charts:**

For glass values that are not listed, linear interpolation is permitted.

Glass properties are based on center of glass values (winter conditions) and are obtained from your glass supplier.

1" GLAZING WITH FIBERGLASS PRESSURE PLATE**System Solar Heat Gain Coefficient (SHGC) vs Percent of Vision Area**

Charts are generated per AAMA 507.

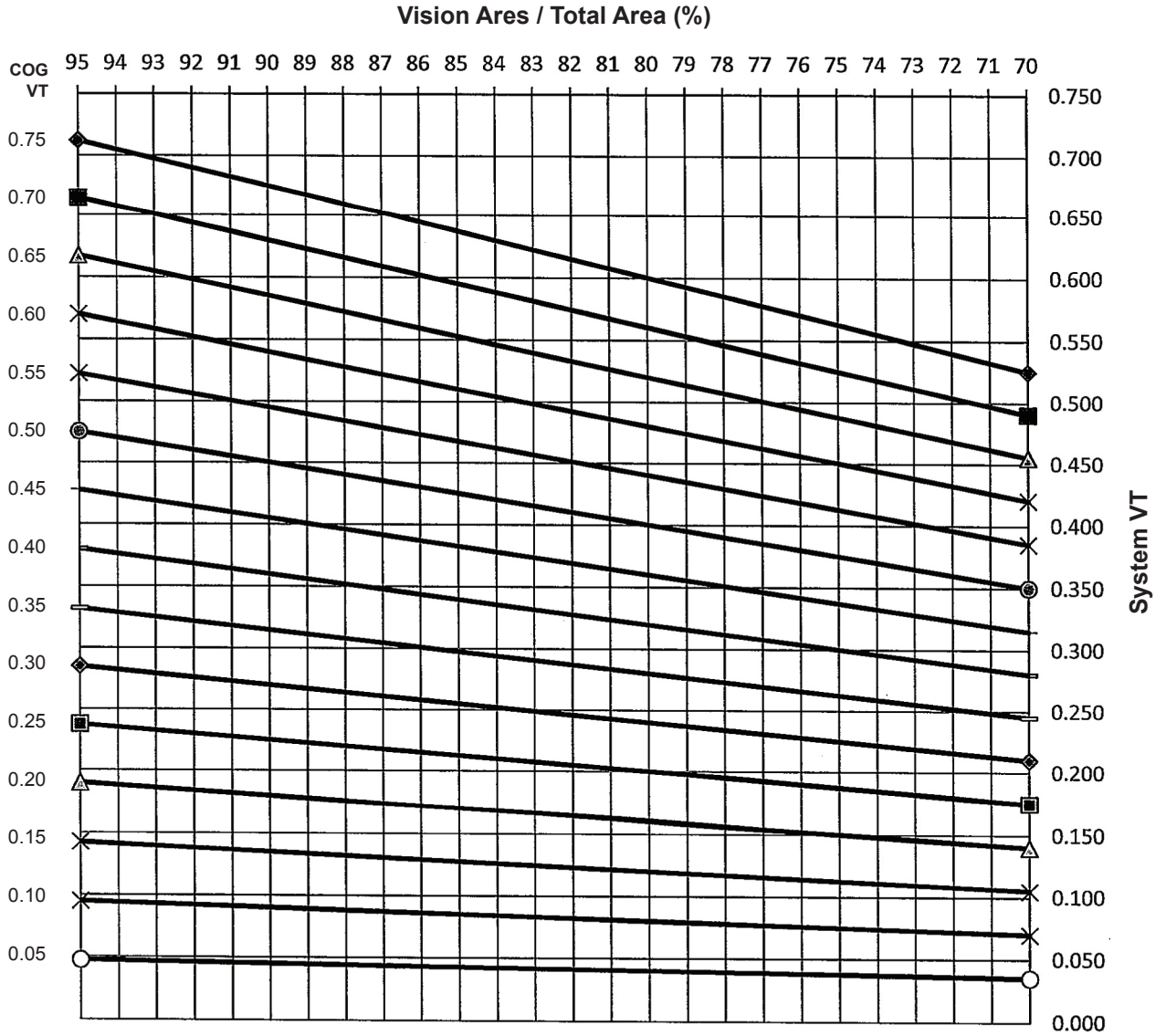
Laws and building and safety codes governing the design and use of glazed entrance, window, and curtain wall products vary widely. Kawneer does not control the selection of product configurations, operating hardware, or glazing materials, and assumes no responsibility therefor.

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1" GLAZING WITH FIBERGLASS PRESSURE PLATE

System Visible Transmittance (VT) vs Percent of Vision Area



Charts are generated per AAMA 507.

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Thermal Transmittance¹ (BTU/hr • ft² • °F)

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0.48	0.54
0.46	0.53
0.44	0.51
0.42	0.49
0.40	0.48
0.38	0.46
0.36	0.44
0.34	0.42
0.32	0.41
0.30	0.39
0.28	0.37
0.26	0.36
0.24	0.34
0.22	0.32
0.20	0.31

**1" GLAZING WITH
FIBERGLASS PRESSURE PLATE**

NOTE: For glass values that are not listed, linear interpolation is permitted.

1. U-Factors are determined in accordance with NFRC 100.
2. SHGC and VT values are determined in accordance with NFRC 200.
3. Glass properties are based on center of glass values and are obtained from your glass supplier.
4. Overall U-Factor, SHGC, and VT Matricies are based on the standard NFRC specimen size of 2,000 mm wide by 2,000 mm high (78-3/4" by 78-3/4").

SHGC Matrix²

Glass SHGC ³	Overall SHGC ⁴
0.75	0.73
0.70	0.69
0.65	0.64
0.60	0.60
0.55	0.55
0.50	0.51
0.45	0.46
0.40	0.42
0.35	0.37
0.30	0.33
0.25	0.28
0.20	0.24
0.15	0.19
0.10	0.15
0.05	0.10

Visible Transmittance²

Glass VT ³	Overall VT ⁴
0.75	0.68
0.70	0.63
0.65	0.59
0.60	0.54
0.55	0.50
0.50	0.45
0.45	0.41
0.40	0.36
0.35	0.32
0.30	0.27
0.25	0.23
0.20	0.18
0.15	0.14
0.10	0.09
0.05	0.05

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